

الجامعة الكوفة  
قسم هندسة البناء والانشاءات  
فرع الهندسة الإنشائية

مشروع تحليل وتصميم بناية باستخدام برنامج

**STAAD PRO V8i**

و برنامج المخططات الإنشائية بواسطة برنامج

**AutoCAD**

مستخرج التخرج السنوي من قسم هندسة البناء والانشاءات  
كجزء من متطلبات نيل شهادة البكالوريوس

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٢٠١١

بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ

((وقال الذين اوتوا العلم ويليكم ثواب الله خير لمن

امن وعمل صالحا ولا يلقاها الا الصابرون))

صدق الله العظيم

# شكر وتقدير

أتقدم بشكري وتقديري وامتنالي الى استاذي الفاضل

**الدكتور علاء كمال عبد الكريم**

لما قدمه لي من جهد وتوجيه

وارشادني بكل اخلاص لأقدم بحثي هذا

والذي اضعه بين يدة ثمرة طيبة لجهودك الكريمه

واتقدم بشكري وتقديري الى كل الاساتذة الذين ساهموا في وصولنا الى هذه  
المرحلة

مع خالص امتنالي الى كل من ساهم في مساعدتي تقديم هذا البحث

والله ولي التوفيق

# الإهداء

الى من كان دعاءها دليلى في ظلمتي  
الى التي نرقت الدموع من اجلي  
الى يسوع الحنان و القلب الطيب الوفي  
الى نبض قلبي امي.....

الى الذين علموني كيف امسك القلم و زهدوا بعملهم لاجلي  
الى من ابصرني بدروب الحياة و اثار امامي معالم الطريق  
الى من وقف الى جانبي ومنحني من علمة و فضلة و توجيهه  
الى اساتذتي مع فائق حبي و تقديرى.....

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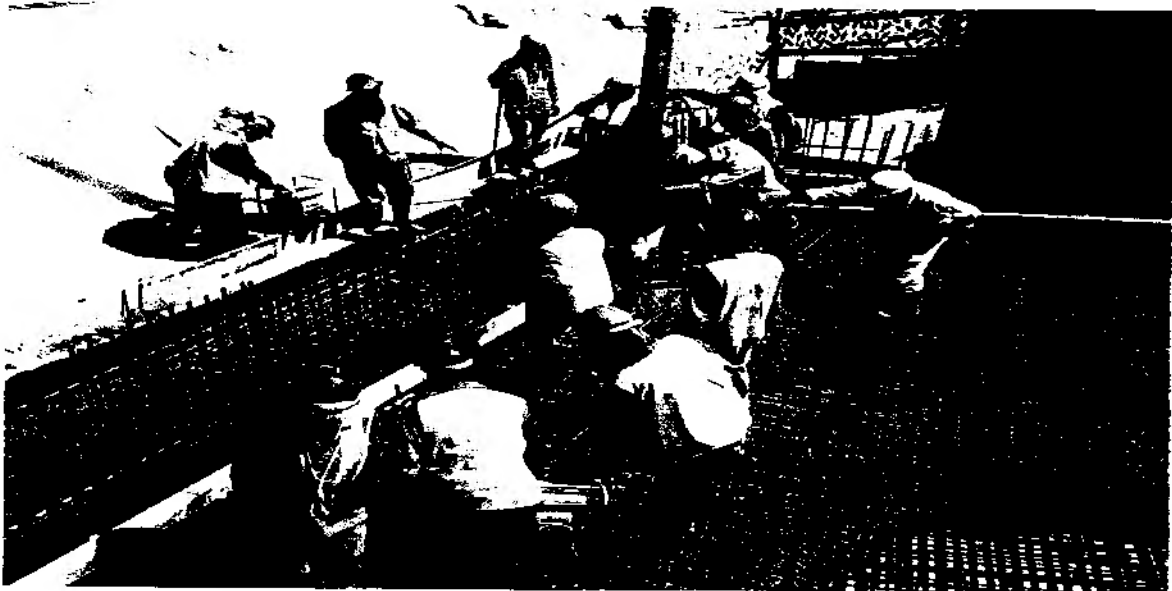
تقسم الابنية الى انواع وفق ما يلي

## ١-١-١ حسب طريقة التنفيذ

### انجاز مرتفعي

يتم تنفيذ كافة فقرات الاعمال تقريبا في موقع العمل ويحتاج هذا الاسلوب في البناء الى ايدي عاملة كثيرة و متعددة الاصناف ، ويستوجب تهيئة و تصنيف المواد بصورة كلية او جزئية.

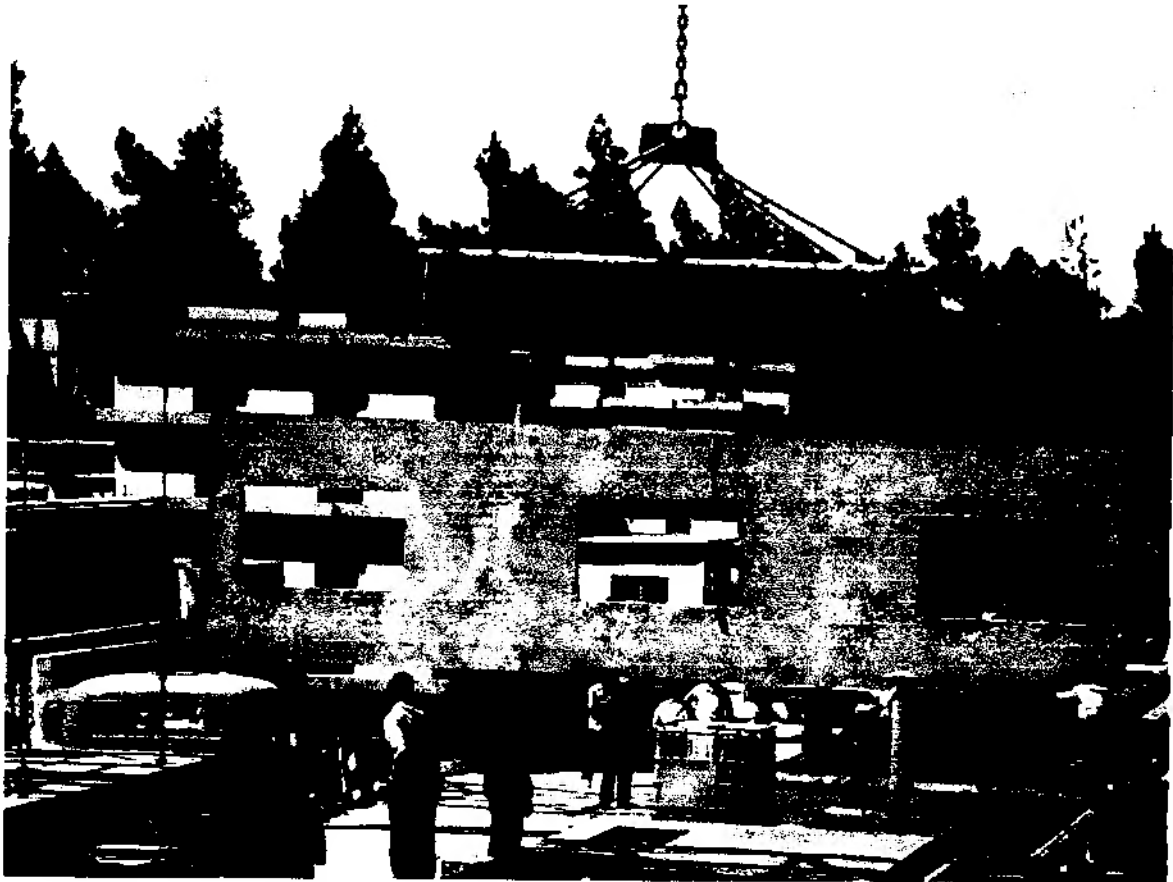
ان مجال تصرف المهندس المصمم في هذا النوع من الابنية واسع الحرية في اختيار الاشكال و المواد المناسبة ، من سلبيات هذا النوع بالتنفيذ تكون نسبة تلف المواد الاولية عالية وسرعة انجازه بطيئة مقارنة مع بقية انواع التنفيذ.



## صب جاهز

ينفذ هذا النوع باستخدام وحدات انشائية جاهزة مصنوعة في معامل متخصصة تكون خارج الموقع في معظم الحالات وتركب هذه الوحدات في موقع العمل بموجب اساليب وتفصيل هندسية معينة.

توجد انواع متعددة من البناء الجاهز بنسب مختلفة من التصنيع خارج موقع العمل و تختلف اساليب تصنيع البناء حسب المواد المستعملة فقد يكون البناء خرسانيا ، معدنيا ، بلاستيكيا او مركبا من عدة مواد مختلفة .





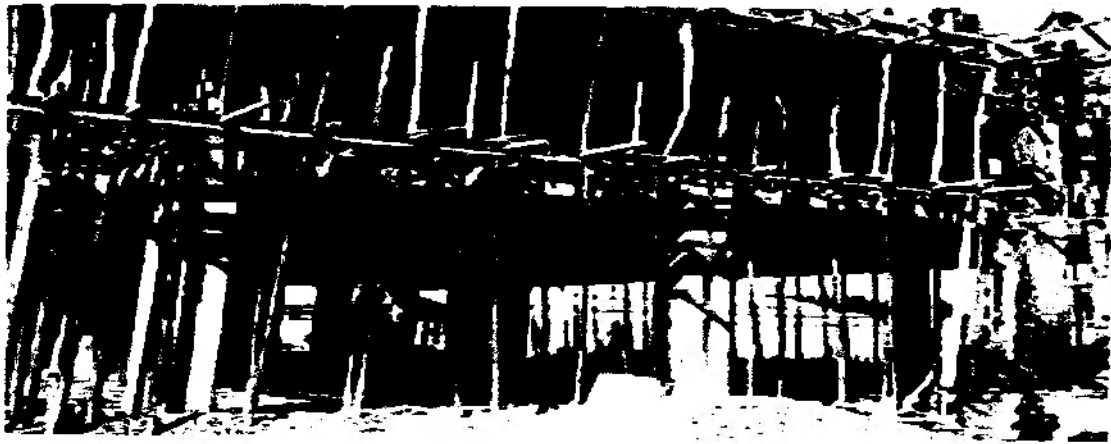
ان المعادن تتحمل اجهادات الشد والربط بدرجة عالية مما يجعل مساحة المقطع المطلوب اصغر مقارنة مع المواد الاخرى و بهذا يقلل من الاحمال النازلة على الاساس ويوفر من المساحات التي تشغلها الاعمدة بفضاء راسي اكبر لهذا فان المنشآت المعدنية اصبحت تستخدم في الابنية المتعددة الطوابق و الابنية ذات الفضاءات الواسعة جدا مثل ابنية المصانع والمخازن والمعارض وغيرها و تحتاج الهياكل المعدنية الى وقاية مستمرة من الحريق وكذلك تآثر بالظروف الجوية.

ان وجوب التزام المصمم بالمقاطع القياسية المنتجة والمتوفرة يحد كثيرا من تصرف الهندسي في التصميم وفي الوقت الحاضر تستورد كافة المقاطع المعدنية المستعملة في البناء لذا يكون هذا النوع من البناء ذو كلف عالية.



الهياكل الخرسانية المسلحة تكون اما مصبوبة موقعا او مسبقة الصب وتتميز الهيكل الخرسانية المسلحة بانه جميع موادها مصنعة محليا ماعدا حديد التسليح . و تعطي الهياكل الخرسانية للمصمم حرية التصرف في انتاج الانماط البنائية و الاشكال المرغوب بها و تتميز بقاومتها للحريق وكذلك بدوامها العالي و بثقل وزنها ويستغرق زمن انشاءها زمنا طويلا بالمقارنة مع الهياكل المعدنية و تحتاج الى سيطرة نوعية في الانتاج والتنفيذ و تكون هذه الهياكل دائمية لا يمكن رفعها او نصبها في مكان اخر.

تنفذ الجدران في الابنية الهيكلية بعد اكمال الهيكل ويمكن رفع الجدران من دون تأثير على سلامة المنشأ .



## البناء غير الهيكلية

تنقل احمال الارضيات في هذا النوع من البناء الى الاسس بواسطة جدران حاملة للانتقال لا يمكن رفعها بعد البناء بخلاف البناء الهيكلية و يتبع هذا الاسلوب في الابنية الاعتيادية ذات الطوابق القليلة لانه تعدد الطوابق يعني زيادة سمك الجدران الامر الذي يؤدي الى نقصان المساحات الصافية للطوابق وتسلط احمال كبيرة على الاساس ويجب ان تبني الجدران الحاملة قبل بناء السقوف و الارضيات.

## البناء المشترك

في هذا النوع هناك اعمدة واعتاب خرسانية او معدنية تعمل كهيكل في جزء من البناء وايضا جدران حاملة في بعض الاجزاء الاخرى ويتبع هذا الاسلوب لتنفيذ متطلبات معمارية و انشائية لاسباب اقتصادية ايضا ومن الضروري توفير التفاصيل الانشائية و اعداد التصميم بشكل ملائم لتجنب الهبوط التفاضلي للاسس اكثر من الحد المسموح به .

## ٢-١ عناصر البناء الهيكلي

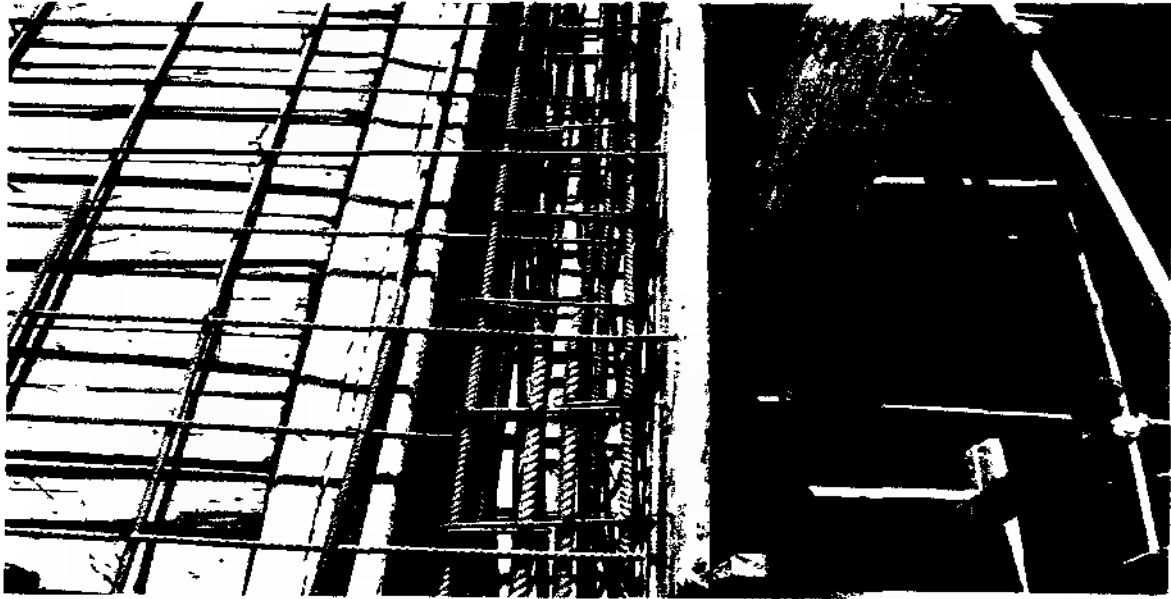
يتكون البناء الهيكلي الخرساني من ثلاثة عناصر رئيسية والتي يتكون من مجموعها الهيكل العام للابنية المختلفة سواء كانت صناعية ،سكنية ،تعليمية ام صحية ذات طابق واحد او متعددة الطوابق مع استعمال المواد المختلفة في انشائها كالحديد والخشب والخرسانة المسلحة وسنقتصر على بيان عمل وتفاصيل البناء باستعمال الخرسانة المسلحة المصبوبة موقعا.

ان النظام الهيكلي في الانشاء يتميز بميزات كثيرة لا تتوفر في غيره من الانظمة البنائية الاخرى كنظام الجدران المحملة للاتقال مثلا حيث يعطي مرونة كبيرة في تقسيم الفضاءات الداخلية وحسبما تتطلبها التصاميم المعدة لها كما ان بالامكان تغير حجوم هذه الفضاءات لمرات كثيرة اذا تطلب الامر اعادة تصميم القواطع الداخلية لانها عناصر غير انشائية بل اجزاء لقسم الفضاءات الداخلية ولا تتحمل اي نوع من الاتقال سوى نقل نفسها فقط اما الاتقال الانشائية فيتحملها الهيكل العام للابنية باختلاف انواعها من اتقال ثابتة او متحركة.



ان هذه المرونة لا تتوفر في غيره من الانظمة الانشائية الاخرى كالبناء باستعمال الجدران الحاملة للاتقال كنظام انشائي في تشييد الابنية حيث لا يمكن رفع او تغيير

ان ارتفاع الروافد يجب ان لا يقل عن النسبة (٢٠/١) من المسافة الفاصل بين الاعمدة و في حالة عداد التصاميم الاولى لاي مشروع من قبل المهندس فان ارتفاعها يقدر بنسبة (١٠/١) من مسافة الفضاء الفاصل بين الاعمدة كتقدير اولي لها في حين يتراوح سمك هذه الروافد من (٣-١/١) من ارتفاعها وبصورة عامة فان هذه النسب هي تقديرات اولية لارتفاع و سمك الروافد الخرسانية ولكنها يجب ان يتم تصميمها حسب الانتقال المسلطة عليها.

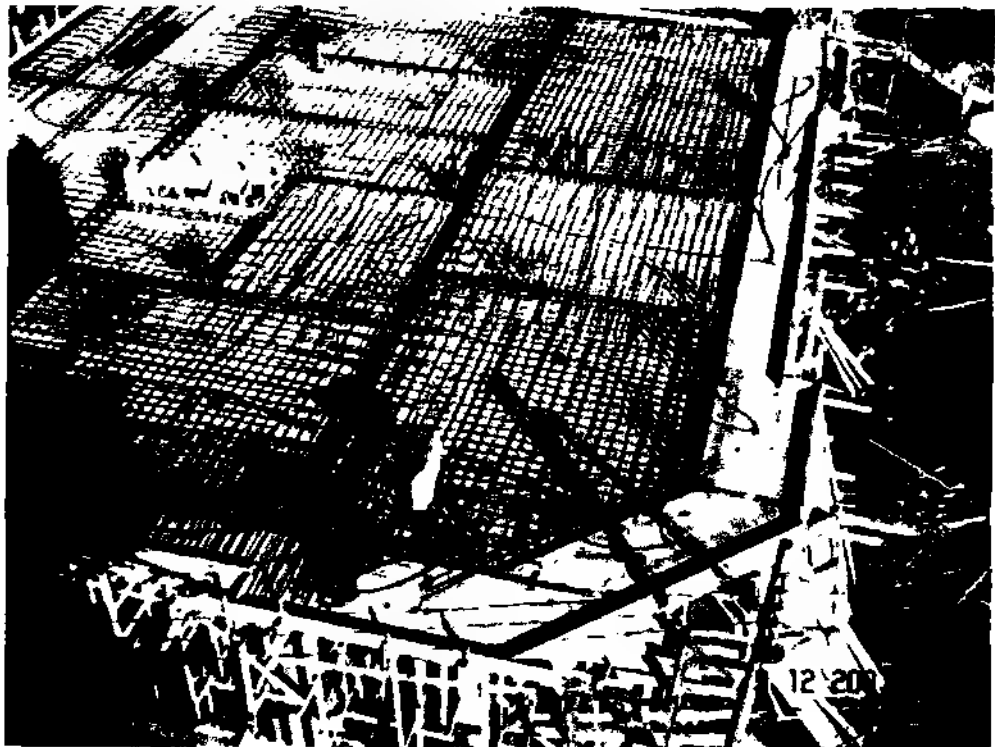


ان هنالك انواع مختلفة من الروافد المصبوبة موقعيا منها الروافد الاعتيادية والتي يكون موقعها اسفل الصبة الخرسانية للسقف اما النوع الثاني هي الروافد الراسية وهي التي يكون موقعها اعلى الصبة الخرسانية للسقف و تستعمل في الفضاءات الكبيرة ذات الطابق الواحد ذلك لعدم امكانية استعمال السقف كارضيات للطوابق العليا لوجود هذه الروافد ام النوع الاخر فهي الروابط المخفية وهي التي يتم تصميمها لتكون جزء من الصبة الخرسانية للسقف .

## الارضيات و السقف Floors & Roof slabs

هي الاجزاء الافقية بالنسبة للابنية المختلفة حيث تجلس هذه الاجزاء فوق الروافد التي تربط الاعمدة مع بعضها لتقسم الابنية بواسطتها الى طوابق متعددة حيث يتم عملها من الخرسانة المسلحة و التي يكون تسليحها باتجاه واحد عندما تكون الصبة الخرائية تستند على الروافد من الجانبين او تكون مسلحة باتجاهين متعاكسين عندما تكون من الصبة الخرسانية مستندة على الروافد الاربعة التي تحيط بالفضاء.

ان هذه الارضيات و السقوف تقوم بنقل و تحميل جميع الاثقال و القوى المسلطة عليها و المتكونة من الاثقال الناتجة من وزن الارضيات والسقوف نفسها والاثقال الثابتة من مواد الانهاء و الاثاث الثابت ليتم نقلها الى الروافد و منها الى الاعمدة التي تقوم بنقلها الى الاساس ومنها الى التربة.



تجعلها تتحمل كل العيوب التي بها دون أن تشكل خطراً كبيراً على ساكنيها إلا في حالات الهزات الأرضية والكوارث الطبيعية.



### المباني غير الخرسانية

يندر وجود مبان متوسطة العمر أو حديثة العمر غير خرسانية في المشرق العربي ، بينما قد تتوفر في المغرب العربي مبان حديثة ومتوسطة العمر تعتمد على جدران حاملة من الحجارة أما الأساسات والأسقف فهي من الخرسانة المسلحة ، كذلك قد يوجد في النادر بعض المباني التي تقام على جدران حاملة من الطوب بأنواعه المختلفة وبقيّة الهيكل من الخرسانة المسلحة .

أما النوع الآخر من المباني الحديثة غير الخرسانية فهو البناء من الفولاذ الصلب وقد نجد عدداً لا بأس به من هذه المباني في بعض عواصم الدول العربية والمدن الهامة بها وسوف لن نتطرق إليه المباني الخرسانية.

معظم المباني الخرسانية في العالم العربي الصغيرة منها والكبيرة لها النظام الإنشائي نفسه وهو عبارة عن هيكل من الأعمدة والحواجز والبلاطات التي تستند في الغالب على رقاب للأعمدة وجسور أرضية تنتهي إلى الأساسات المنفردة أو المستمرة أو

الحصائر وتستخدم الأوتاد في بعض الأبنية التي تتطلب تربتها مثل هذا النوع من الأساسات أنواع التصدعات وأسبابها في العالم العربي يفتقر العالم العربي على المستوى القطري والإقليمي والعربي على السواء إلى قاعدة للبيانات في المجالات المختلفة تحتوي على التجارب والأبحاث والخبرات التي توفر للباحث المعلومات الضرورية التي يحتاجها في هذا البحث أو ذاك وتساعد على التنسيق وتفاذي الإزدواجية.

لذلك فمن الصعب جداً على المرء أن يعمم تجارب مدينة أو منطقة على قطر ويصعب كذلك تعميم تجارب بلد على عدة بلدان وستبقى هذه المشكلة حتى توجد مثل هذه القاعدة العامة للمعلومات التي يمكن الاستعانة بها على المستوى القطري والإقليمي والعربي ولم يكن لي من حيلة في الوصول إلى بعض التعميم حول موضوع التصدعات وأسبابها في العالم العربي إلا من خلال الاستعانة بمجلد البحوث الخاص بندوة تصدعات المباني في العالم العربي.



Figure 15. RC frame building with masonry infills in Algeria (after Dr. 2003 Roumenos earthquake). (a) masonry infill walls fail in both directions (b) Masonry infill wall failure during diagonal cracking due to compression-straction (plates 5, Bree)

# تصدعات المباني في العالم العربي

تأتي في المرتبة الأولى سوء التنفيذ يلي ذلك التصدعات التي تحدث بفعل العوامل الجوية والظروف البيئية المحيطة مثل تصدعات الإنكماش والحرارة والتشققات الذاتية والتي تحدث في الخرسانة في عمرها الأول وهي الأخرى تعد تنفيذية في غالبيتها ، ومن هذا يمكن القول أن أكثر من ٥٠ % من التشققات تحدث بسبب سوء التنفيذ و النقاط التالية تبين بعض أسبابها

## أسباب تتعلق بسوء التنفيذ

- ١- استعمال مواد أولية رديئة ولا تطابق المواصفات واستعمال خرسانة فقيرة وضعيفة ومقاومتها أقل بكثير من المطلوب في مواصفات المشروع.
- ٢- تقليل كمية التسليح وتقليل عرض القطاعات وسمكها.
- ٣- عدم مراعاة الظروف المناخية والبيئية المؤثرة وعدم أخذ الاحتياطات لفروق درجات الحرارة بين الخرسانة والجو الخارجي وخاصة عند صب كميات ضخمة من الخرسانة.
- ٤- إهمال الدعم الجيد للشدات وعدم مراعاة أصول الصناعة والمواصفات في كيفية تثبيتها وخاصة عند إنشاء الأتربة ، وفي بعض الحالات إزالة الشدات قبل حصول الخرسانة على المقاومة المطلوبة.
- ٥- إضافة أحمال جديدة فوق البلاطات أو الجسور أو الأعمدة دون مراعاة لما تتطلبه من حلول إنشائية صحيحة.
- ٦- إهمال التصريف الصحيح لمياه الأمطار وسوء تنفيذ الميول والصرف الصحي وعدم العزل الجيد للأنايب.
- ٧- إهمال أنظمة ضبط الجودة ومراقبتها في المصنع والموقع.



٨- عدم اختيار جهاز الإشراف الجيد والمقاول الكفاء القادرين على استدراك الأخطاء وحل مشكلات التنفيذ.

٩- سوء اختيار أماكن الفواصل وتنفيذ بعضها وإهمال الآخر.

١٠- زيادة تحميل الأعضاء الخرسانية في عمرها الأول عما تتحمله مقاومتها كخزين مواد الإنشاء ومعدات التشييد.

١١- قطع قضبان التسليح وإيجاد فتحات في الخرسانة لم تؤخذ في التصميم الإنشائي.

١٢- فقدان الاهتمام والعناية بنقل ورفع وتركيب وتثبيت الوحدات مسبقة الصنع.

وفي المرتبة الثانية تأتي التصدعات التي تنشأ بسبب مشكلة في ميكانيكا التربة وهندسة الأساسات وكثير منها يتعلق بارتفاع المياه الجوفية ، وتبين النقاط التالية بعض الأسباب التي تؤدي إلى تصدعات في مجال ميكانيكا التربة وهندسة الأساسات.

## أسباب تتعلق بميكانيكا التربة وهندسة الأساسات

١- تربة انتفاخية

٢- تربة انهيارية

٣- دراسات ناقصة وغير متكاملة عن أحوال التربة أو تخمين خاطئ لتحملها ، وإهمال تقارير خبراء التربة

٤- عدم تجانس التربة في المواقع

٥- هبوط التربة مع الزمن

٦- هبوط التربة تحت تأثير التأسيس لمباني مجاورة

٧- ارتفاع منسوب المياه الجوفية أو تأثير الأمطار والمجاري والزراعة والتسربات

٨- ردميات غير مناسبة

٩- تغير خواص التربة بتغير نسبة الرطوبة وارتفاع المياه الجوفية

- ١٠- زيادة الأحمال على الأساسات
- ١١- نسبة أملاح أو كلوريدات وكبريتات عالية
- ١٢- إهمال عزل القواعد والمنشآت التحتية بالشكل المناسب

أما النوع الذي يأتي في المرتبة الثالثة فهو صدأ التسليح والذي يتركز عادةً في المدن الساحلية والقريبة من البحار والأنهار ، ويبين الجدول التالي أهم الأسباب المؤدية إلى صدأ التسليح ومنه نرى أن جزءاً مهماً منها يرجع إلى سوء التنفيذ أو قصور التصميم فيما يخص الخرسانة والغطاء الخرساني.

## أسباب تتعلق بصدأ حديد التسليح

- ١- توفر الكلور بكميات كبيرة قريباً من الأسطح الخرسانية.
- ٢- إهمال استعمال العوازل المختلفة التي تمنع أو تحد من تسرب الكلوريدات والرطوبة والهواء إلى داخل الخرسانة.
- ٣- زيادة نسبة الكلوريدات في الهواء أو الوسط من حول الخرسانة.
- ٤- تخزين المواد الكيميائية التي تعمل على صدأ التسليح.
- ٥- إهمال وقصور في تصميم وتنفيذ الغطاء الخرساني المطلوب
- ٦- ضعف الخرسانة
- ٧- زيادة نسبة الماء/الاسمنت.
- ٨- إهمال احتياطات الجو الحار والظروف البيئية الأخرى وأثر الحرارة على تعجيل التفاعلات الكهروكيميائية.
- ٩- رشوحات وتسربات التمديدات الصحية وغيرها
- ١٠- مياه الأمطار والمياه الجوفية ومياه الري والزراعة وغيرها
- ١١- المد والجزر
- ١٢- احتواء الحصى وماء الخلطة على نسبة عالية من الكلوريدات
- ١٣- انخفاض نسبة الاسمنت عن الحد الأدنى لها.

- ١٤- تطبيق المواصفات الأجنبية دون النظر إلى الظروف البيئية المختلفة
- ١٥- إهمال ضبط الجودة ومراقبتها بالنسبة للخرسانة وموادها.
- ١٦- ترك العناية بالمعالجة للأسطح الخرسانية المختلفة مما يساعد على وجود الانكماش والتشققات الحرارية التي تساعد على تسرب الأملاح والرطوبة والهواء إلى داخل الخرسانة.



وفي المرتبتين الأخيرتين قصور التصميم والكوارث الطبيعية ، وتبين النقاط التالية بعض الأخطاء في التصميم التي تؤدي إلى تصدعات في المباني.

### أسباب تتعلق بأخطاء التصميم

- ١- عدم شمول المخططات والمواصفات للتفاصيل الضرورية واللازمة لحسن التنفيذ
- ٢- الاعتماد على مواصفات عالمية أو أجنبية قد لا تتناسب مع ظروف البلد وكفاءة العمال وطريقة التنفيذ
- ٣- اختيار مخططات نموذجية للعمائر أو للبيوت السكنية وتنفيذها في مناطق مختلفة دون مراعاة ظروف كل موقع
- ٤- اختيار مواد غير مناسبة أو صعوبة التنفيذ مع توفر المواد التي تعطي إمكانات أكبر وكذلك استخدام المواد في غير موضعها كاستخدام التسليح عالي المقاومة مع خرسانة ضعيفة جداً

- ٥- إغفال حساب بعض القوى الأفقية التي تنشأ من أشكال المباني
- ٦- إهمال توفير التسليح اللازم لمقاومة الانكماش والإجهادات الحرارية
- ٧- عدم تصميم الغطاء الخرساني بما يتناسب وظروف المنشأ والبيئة المحيطة
- ٨- عدم اختيار الاستشاري أو المهندس الكفاء للقيام بعملية التصميم
- ٩- النقص في مقاسات العناصر الإنشائية وتسليحها لمقاومة الأحمال والعزوم والقص .

لاستكمال الموضوع من جوانبه كافةً نورد النقاط التالية الذي يبين بعض أسباب التصدعات التي ترجع إلى سوء الاستعمال وإهمال الصيانة.

### **أسباب تتعلّق بسوء استعمال المباني**

- ١- زيادة الطوابق في المباني أو دور السكن القديمة
- ٢- تغطية الفرق في اختلاف المناسيب بكميات من الرمل لها أوزان كبيرة
- ٣- زيادة الأحمال نتيجة لأعمال الترميم كزيادة سمك البلاطة والطبقة العازلة لتفادي تسرب المياه والتخزين السيء لمواد الترميم فوق المبنى
- ٤- تغيير الغرض الذي أنشأ من أجله المبنى مثل أن يتحول مبنى سكني إلى مدرسة
- ٥- فقدان الصيانة الدورية والوقائية والعلاجية
- ٦- الصيانة والإصلاحات الخاطئة
- ٧- الصيانة المتأخرة بعد فوات الأوان واستفحال الأضرار

# الفصل الثالث الحكم الثاني

• الاحمال الميتة (dead load)

• الاحمال الحية (live load)

٧- يقوم البرنامج بتحليل اجزاء وعناصر المنشا حسب طريقة التحليل الانشائي المستخدم

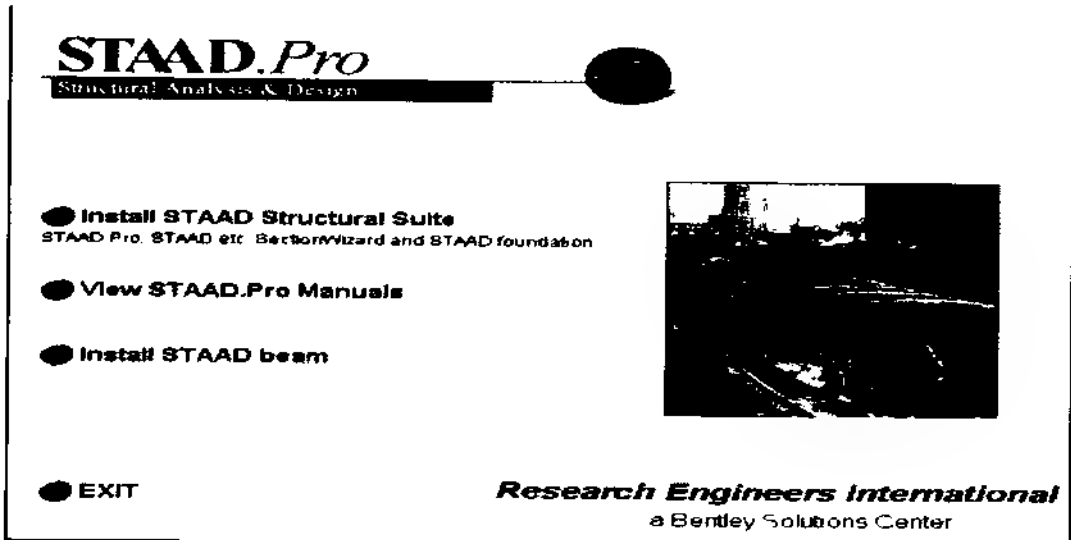
٨- يتم التصميم بالاعتماد على مواصفة عالمية معينة والتي جهز بها البرنامج مثل .ACI CODE

## مميزات Staad pro

١- يحتوي البرنامج على عدد من نماذج المنشآت الجاهزة بقالها العام مع امكانية تعديل كافة المتغيرات للحصول على النموذج باقل جهد ممكن.

٢- يتضمن البرنامج طرق فعالة و ادوات متنوعة لتمثيل المنشآت المعقدة بطريقة ثلاثية الابعاد من خلال واجهة البنائية.

٣- يتميز البرنامج بامكانية القوة في عرض النتائج عدديا و بيانيا كما يتضمن البرنامج برنامجا جزئيا في لعرض التقارير و يتميز البرنامج بامكانيات متقدمة لانشاء التقارير مخصصة و احترافية للمشروع .

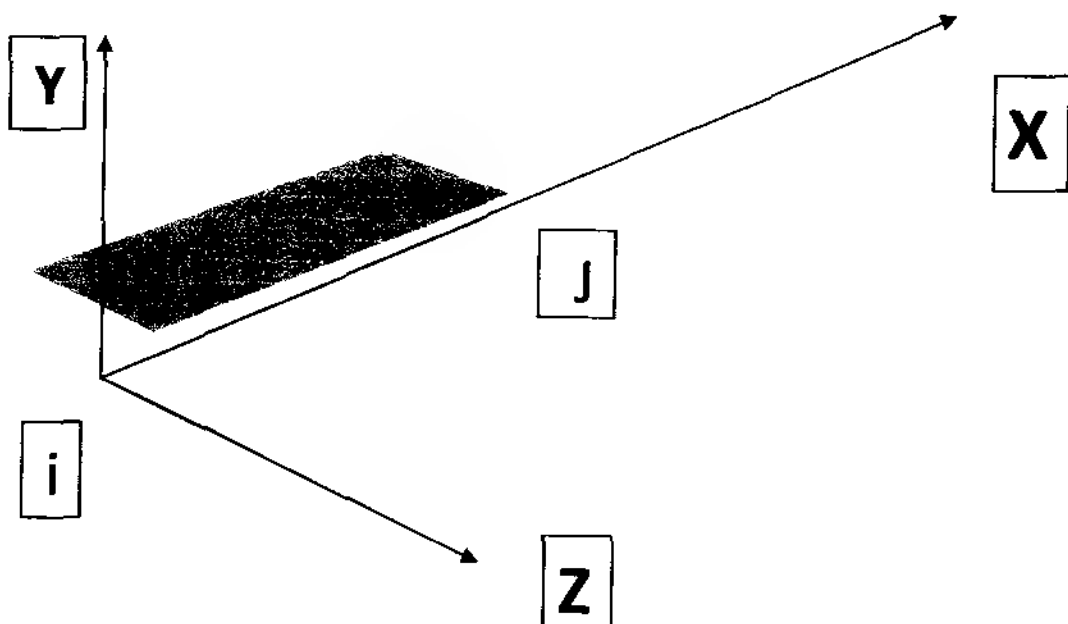


يستخدم **STAAD.PRO** نموذجين من جمل الاحداثيات لتعريف الشكل الهندسي للمنشأ وهما

## الجملة الاحداثيات المحلية **Local Coordinate System**

يقترن مع كل عنصر من عناصر المنشأ جملة من الاحداثيات ديكرتية مستطيلة موضعية او محلية تحقق محاور احداثيات كل جملة محلية قاعدة اليد اليمنى. يظهر الشكل ادناه عنصر جاسى بوصلة بداية (i) و وصلة نهائية (j) ويقترن مع هذا العنصر جملة احداثيات موضعية معرفة بالنسبة الى جملة الاحداثيات الديكرتية وتصف بشكل كاف توضع هذا العنصر بالنسبة للجملة العام .

يحدد الاتجاه المحلي للمحور (X) من الوصلة (i) الى الوصلة (j) ويمكن تطبيق قاعدة اليمنى للحصول على الاتجاه الموجب لكل من المحورين (Y,Z)



## ٢١.١.١ نظام الإحداثيات العالمية Global Coordinate System

يتعامل البرنامج مع ثلاثة نماذج من جمل الاحداثيات العامة لتوصيف الشكل الهندسي للمنشأ وهي

### ١.١.١.١ نظام الإحداثيات الديكارتي التقليدية conventional Cartesian coordinate system

وتتألف جملة الاحداثيات الديكارتي المستطية من نقطة مبدا (o) و ثلاث محاور متعامدة OZ-OY-OX تحقق قاعدة اليد اليمنى ويمكن استخدام هذه الجملة لتعريف نقاط الوصل واتجاهات القوى المطبقة ويرمز للانتقالات وق المحاور الثلاثية بالرمز u1-u2-u3 ويرمز للدورانات بالرمز u4-u5-u6 وفق المحاور OZ-OY-OX على الترتيب.

### ١.١.١.٢ نظام الإحداثيات الأسطوانية Cylindrical Coordinate system

تنشئ هذه الجملة باستبدال المحورين OY-OX في الجملة الديكارتي التقليدية بنصف القطر و الزاوية مقاسة بالدرجات ام المحور OZ مطابقا للمحور OZ في الجملة الديكارتي ويتم تحديد اتجاهه الموجب وفق قاعدة اليد اليمنى.

### ١.١.١.٣ نظام الإحداثيات الأسطوانية العكسية Reverse Cylindrical coordinate system

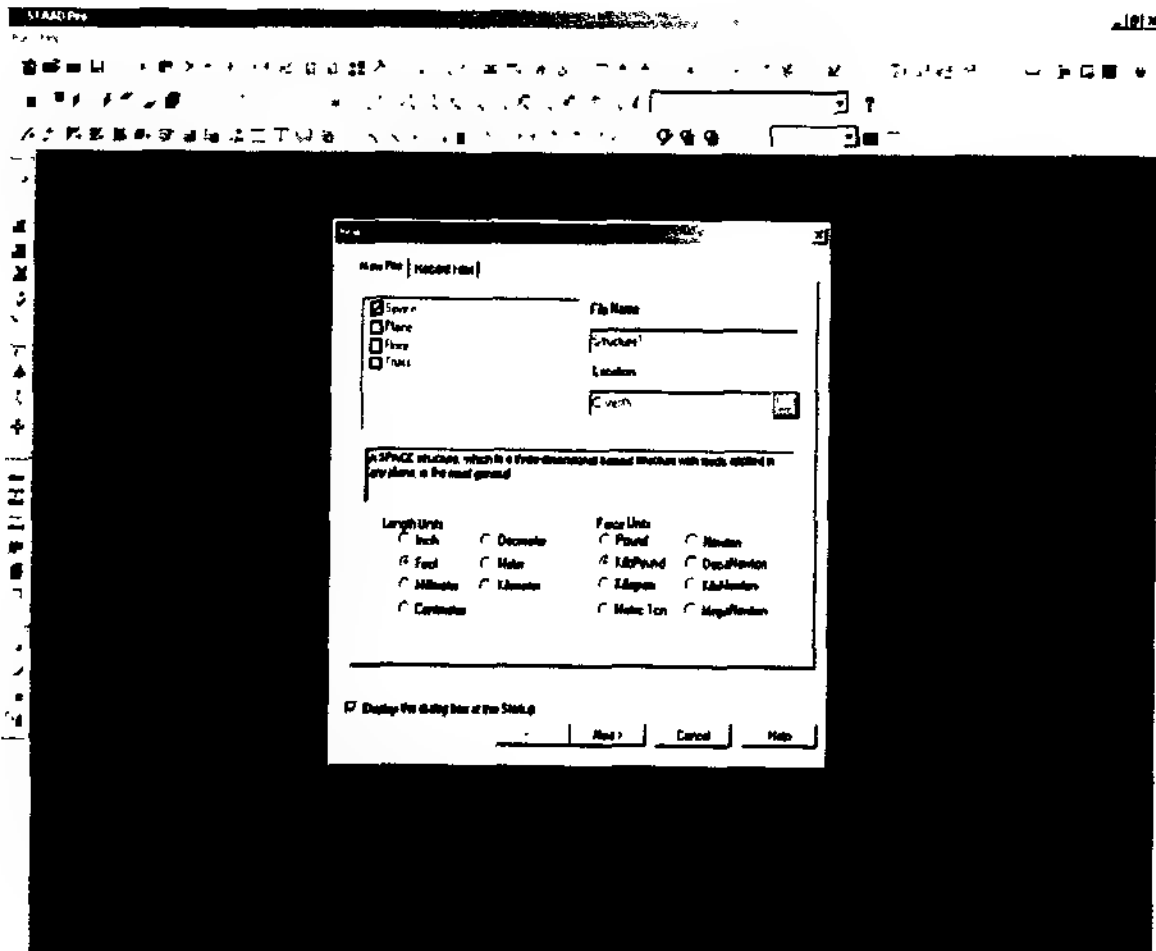
وهي نموذج من الاحداثيات الاسطوانية بحيث يقترن المستوي (r-θ) في هذه الجملة مع المستوي (x-z) من جملة الاحداثيات الديكارتي التقليدية وتطبق قاعدة اليمنى لتعريف الاتجاه الموجب للمحور (y) .



# نماذج المنشآت التي يتوجبها البرنالمج

يتألف المنشأ من مجموعة من العناصر الانشائية تماسك مع بعضها البعض لتؤلف منشأ يقاوم الحمولات التي يتعرض لها والمنشآت هي

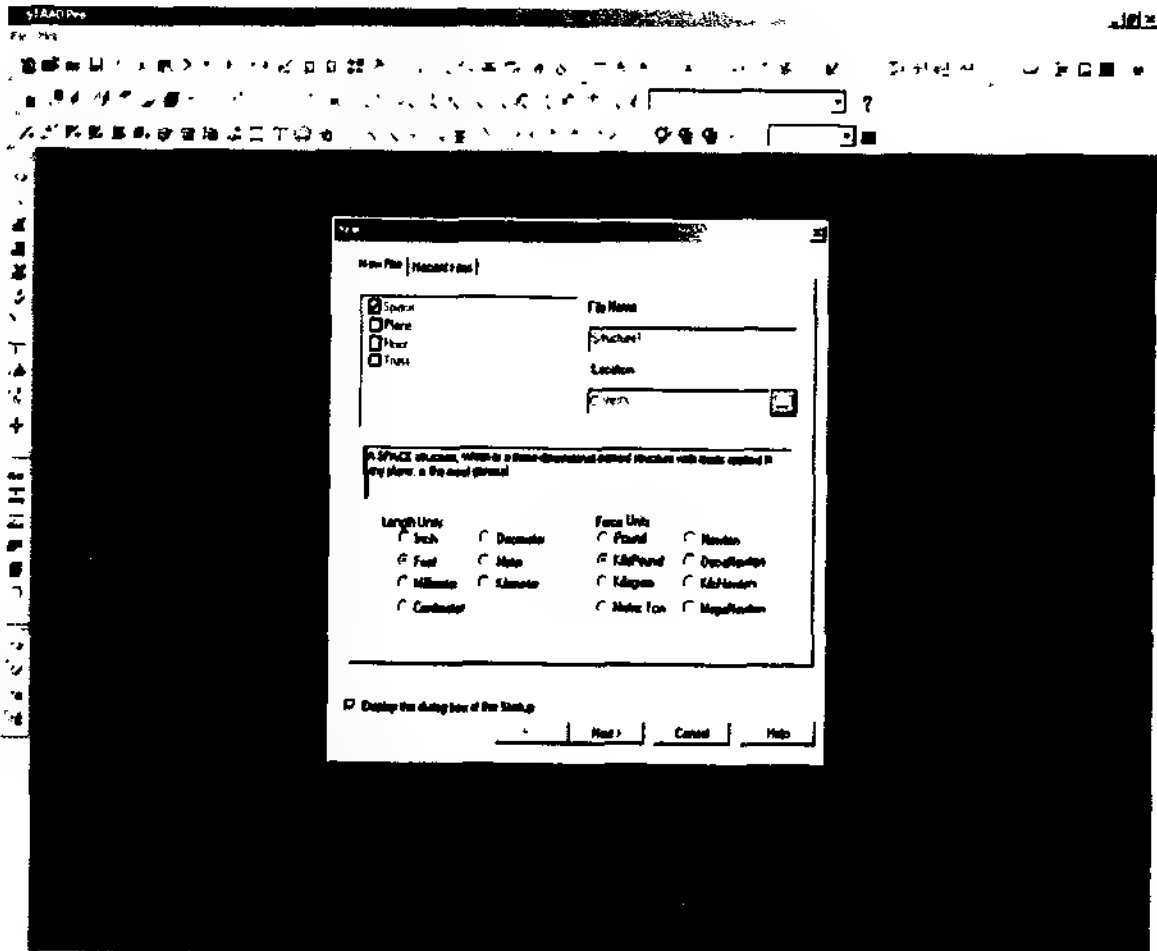
- المنشآت الثلاثية الابعاد Space structure
- المنشآت المستوية plain structure
- المنشآت الشبكية Truss structure
- منشآت الارضيات Floor structure



# نماذج المنشآت التي يعالجها البرنامج

يتألف المنشأ من مجموعة من العناصر الانشائية تماسك مع بعضها البعض لتؤلف منشأ يقاوم الحمولات التي يتعرض لها والمنشآت هي

- المنشآت الثلاثية الابعاد Space structure
- المنشآت المستوية plain structure
- المنشآت الشبكية Truss structure
- منشآت الارضيات Floor structure



## ٢-٢ مصفوفة الصلابة

يعرف المنشأ في طريقة مصفوفة الصلابة بانه مجموعة من اجزاء مرتبطة ببعضها في مفاصل تدعى العقد (node) . ان الاحمال الخارجية تكافى باحمال تكون مسلطة في العقد . ان اعادة ارتباط اجزاء المنشأ في مواقع عقدة تستند على الشروط التالية .

- توازن القوى
- توافق الازاحات
- علاقة القوة بالازاحة

علية فان طريقة مصفوفة الصلابة تعتمد على تجزئة المنشأ الى اجزاء ترتبط ببعضها بعدد محدد من المفاصل التي ندعى العقد . ان الحالة المثلى لتمثيل المنشأ تعتمد على عدد الاجزاء المفروضة و شكلها و ابعادها على ان يكون المنشأ الاصلي ممثلا بالحالة المجزأة التي يجب ان يبقى فيها النموذج الازاحي قريب من الحل الصحيح. ويفترض ان جزء المنشأ مستقيم ومنتظم المقطع، وان خواص مادته ثابتة ، وان يرتبط بالاجاء القريبة منه بواسطة العقد . و نتيجة لذلك فان مواقع العقد يجب ان تكون التي يحصل فيها تغير في الشكل الهندسي او تغير في الاحمال المسلطة او تغير في خواص المادة . ان العلاقة الاساسية التي تربط الاحمال (F) والازاحات ( $\Delta$ ) في النهايات الحرة والصلابة (K) يمكن كتابتها بالشكل التالي

$$F=K * \Delta$$

حيث ان

F :تمثل مصفوفة الاحمال المسلطة على العقد

K :تمثل مصفوفة الصلابة للمنشأ

$\Delta$  : تمثل الازاحات في العقد

# شكل مصفوفة الصلابة الكلية للمنشأ

ان ذلك يعني وضع مصفوفات الصلابة لاجزاء المنشأ الواحد بمصفوفة صلابة واحدة تدعى مصفوفة صلابة المنشأ ويعتمد ذلك على الايفاء بالشرطين التاليين :-

## ١. شرط توازن القوى

ان اي جزء من المنشأ يجب ان يكون في حالة توازن تحت تاثير القوى المؤثرة عليه ، و بالتالي يجب ان يكون المنشأ الكلي في حالة توازن . ان عدد حالات التوازن يعتمد على طبيعة الاجزاء المفروضة في المنشأ و عددها . ومن الملائم وضع حالات التوازن بدلالة القوى المؤثرة على العقد او مفاصل للمنشأ .اي ان مجموع القوى المؤثرة في الجزء تساوي صفر .

## ٢. شرط توافق الازاحات

اذا فرضنا اي عقدة في المنشأ ببعدين لها انحراف في كل من الاحداثيين (x) و (y) و دوران حول الاحداثي (Z) فان ذلك يعني ان هنالك ثلاث ازاحات في العقدة وان هذه الازاحات يجب ان تتوافق مع الازاحات في نهاية اي جزء من الاجزاء المربوطة بالعقدة وفي نقطة الربط.

فاذا كانت (n) دالة على عدد العقد في المنشأ و (m) دالة على عدد درجات الحرية في العقدة الواحدة فان المجموع الكلي لمعادلات التوافق يساوي (m\*n) .

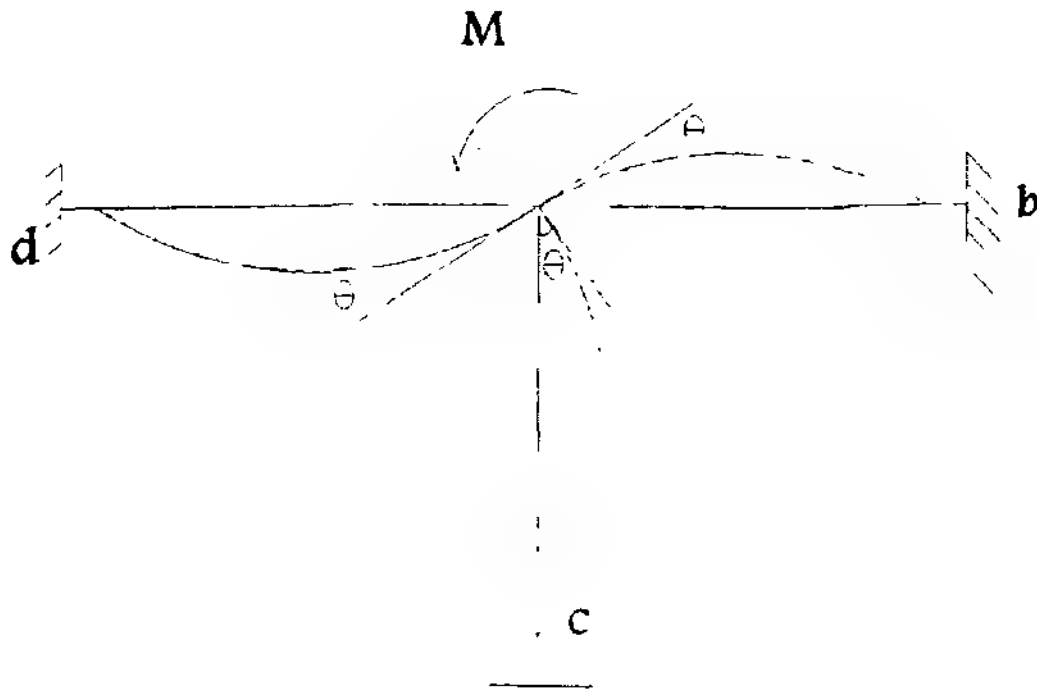
والايفاء بالشرطين المذكورين في اعلاة يمكن وضع مصفوفة صلابة اي جزء من اجزاء المنشأ في موقعها الصحيح في مصفوفة صلابة المنشأ

# درجات حرية الحركة

نذكرنا ان اول خطوة في طريقة مصفوفة الصلابة هي تجزئة المنشأ الى مجموعة من الاجزاء المربوطة مع بعضها بواسطة العقد ويمكن تحديد مواقع العقد في منشأ كما يلي :-

- (١) مواقع المساند
- (٢) نهايات الاجزاء
- (٣) المفاصل في الهياكل والجملونات
- (٤) المواقع التي يتغير فيها المقطع
- (٥) نقاط الاحمال المركزة

بما ان اي منشأ خطي مستمر يكون محتويا على عدد غير محدود من الازاحات . لكن يمكن توضيح الشكل المزاح بعدد محدود من الازاحات . ان هذا العدد المحدود المعروف للشكل المزاح يدعى "عدد درجات حرية الحركة" فمثلا يمكن القول بان الهيكل الموضح بالشكل ادناه له درجة واحدة منحرفة الحركة ممثلة بدوران المفصل (a) بمقدار  $\theta$  وبمعرفة دوران المفصل يمكن احتساب كل القوى الداخلية و معرفة الخط المرن الشكل المزاح اذا اهمل تغير الشكل محوريا ان عدد درجات حرية الحركة لمنشأ يساوي عدد مركبات الازاحة في العقد و بايجاد قيم هذه الازاحات فان ذلك يعني معرفة الشكل المزاح للمنشأ ولذلك ان الاجزاء بين العقد تعتبر منحنيًا مرنا معتمدة على ازاحات نهاياتها و الاحمال المسلطة وخواصها الهندسية.



لمعرفة دوران المفصل يمكن احتساب كل القوى الداخلية ومعرفة الخط المرن للشكل المزاح اذا اهمل تغير الشكل محوريا ان عدد درجات حرية الحركة لمنشأ يساوي عدد مركبات الازاحات في العقد و بايجاد قيم هذه الازاحات فان ذلك يعني معرفة الشكل المزاح للمنشأ.

للمنشآت نوات الابعاد الثلاثة يفرض ان لها ست درجات لحرية الحركة في كل عقدة اما اذا كان المنشأ ذا بعدين فيفرض ان له ثلاث درجات لحرية الحركة في كل عقدة و ان بعض من هذه الدرجات يمكن ان تكون مقيدا بسبب مساند المنشأ او بسبب فرض سلوكية معينة للمنشأ . وعليه فان الدرجات الباقية تكون ممثلة لعدد درجات حرية الحركة .

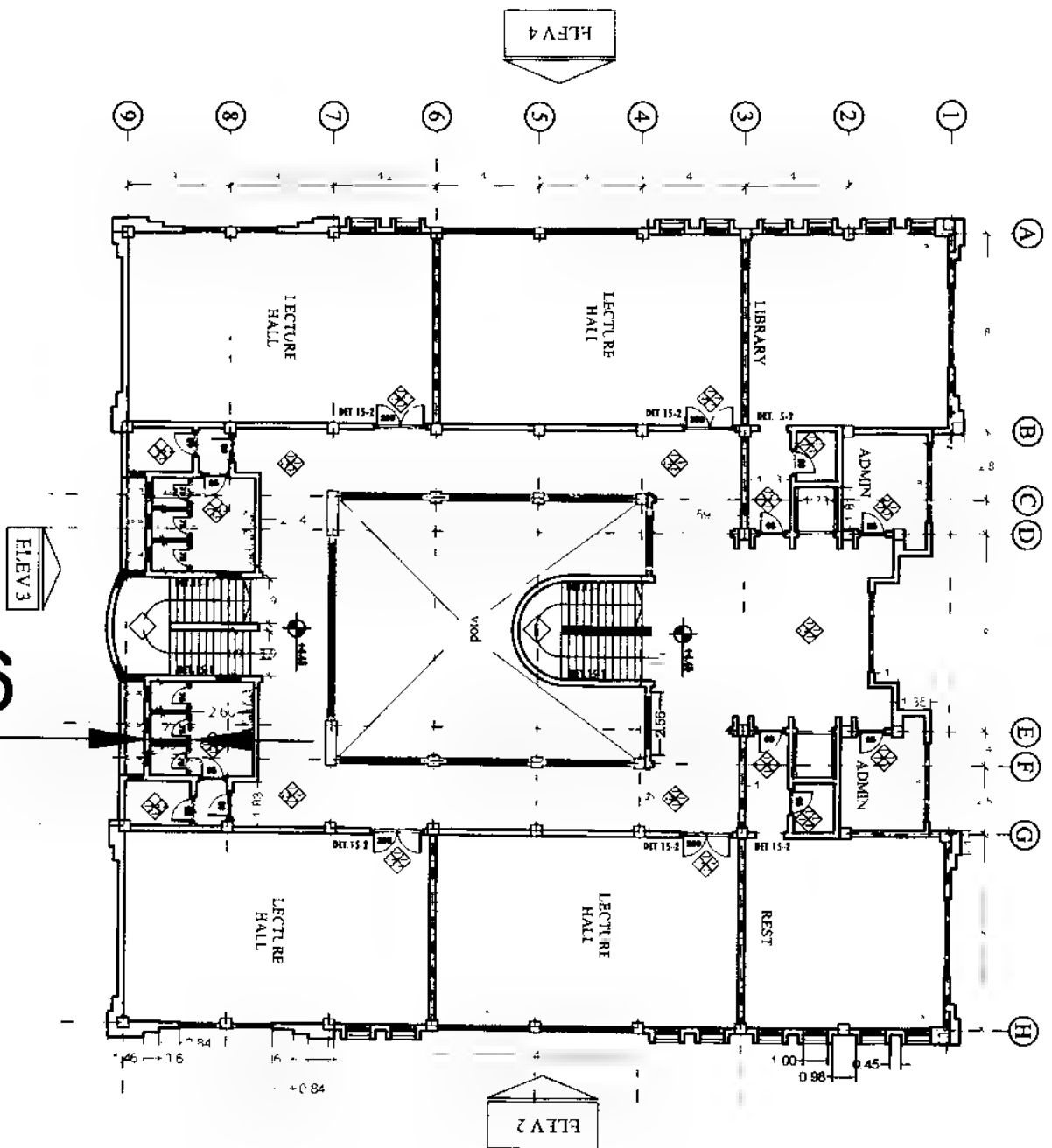
## ١٠٣ وصف البناية

تم اختيار بناية تقع في محافظة بغداد وهي قسم دراسي في الجامعة الاسلامية بمساحة ١١٢٠ متر مربع و البناية تتكون من اربع طوابق و هي مؤلفة من هيكل خرساني من الاعمدة العتبات و البلاطات الخرسانية و تستند البناية الى اساس حصيري.

تم تحليل البناية و تصميمها بالاعتماد على المواصفة الامريكية

(ACI 318M-code) .

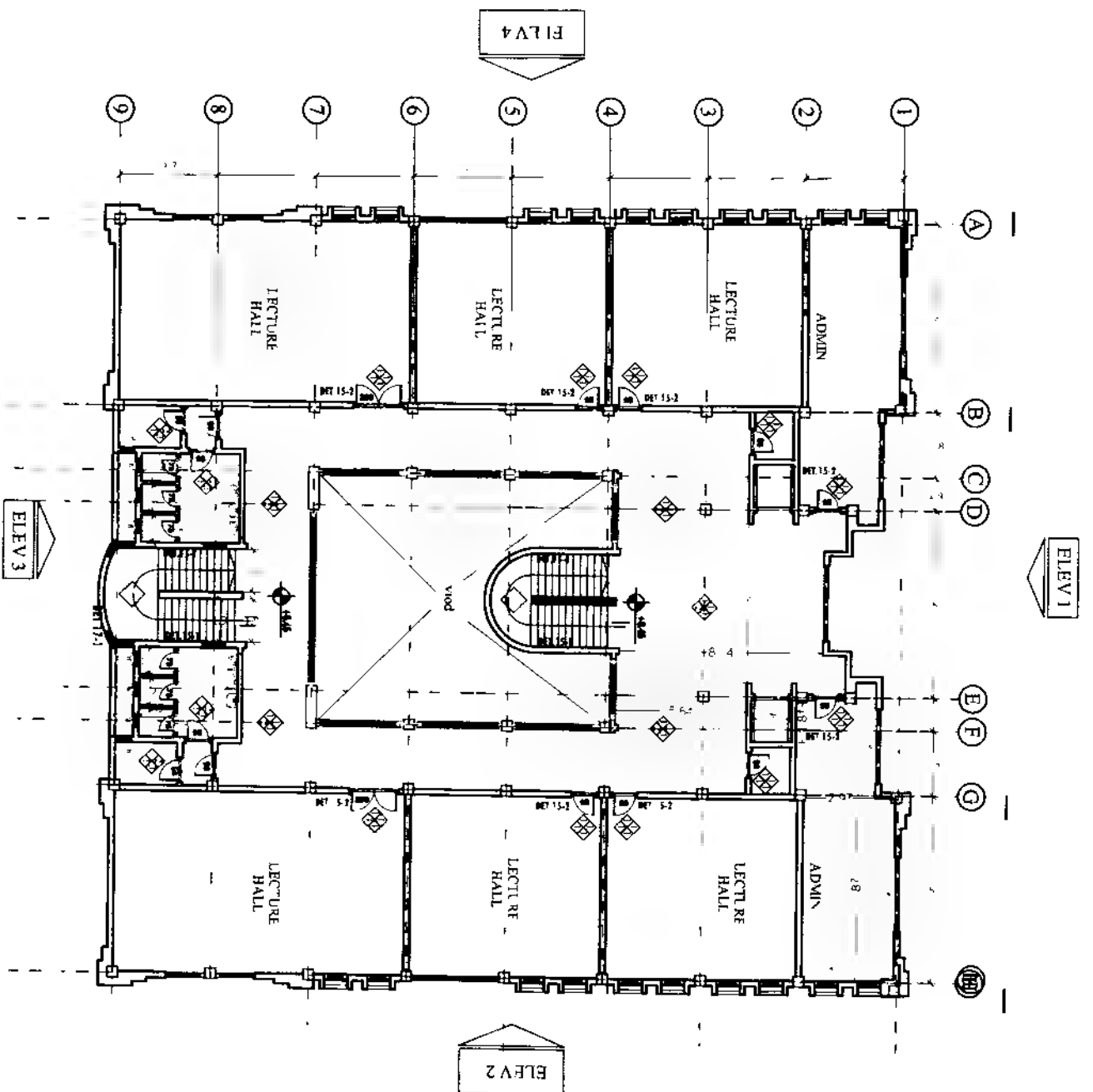
تفاصيل البناية مبينة في المخططات المعمارية التالية :



Notes:-

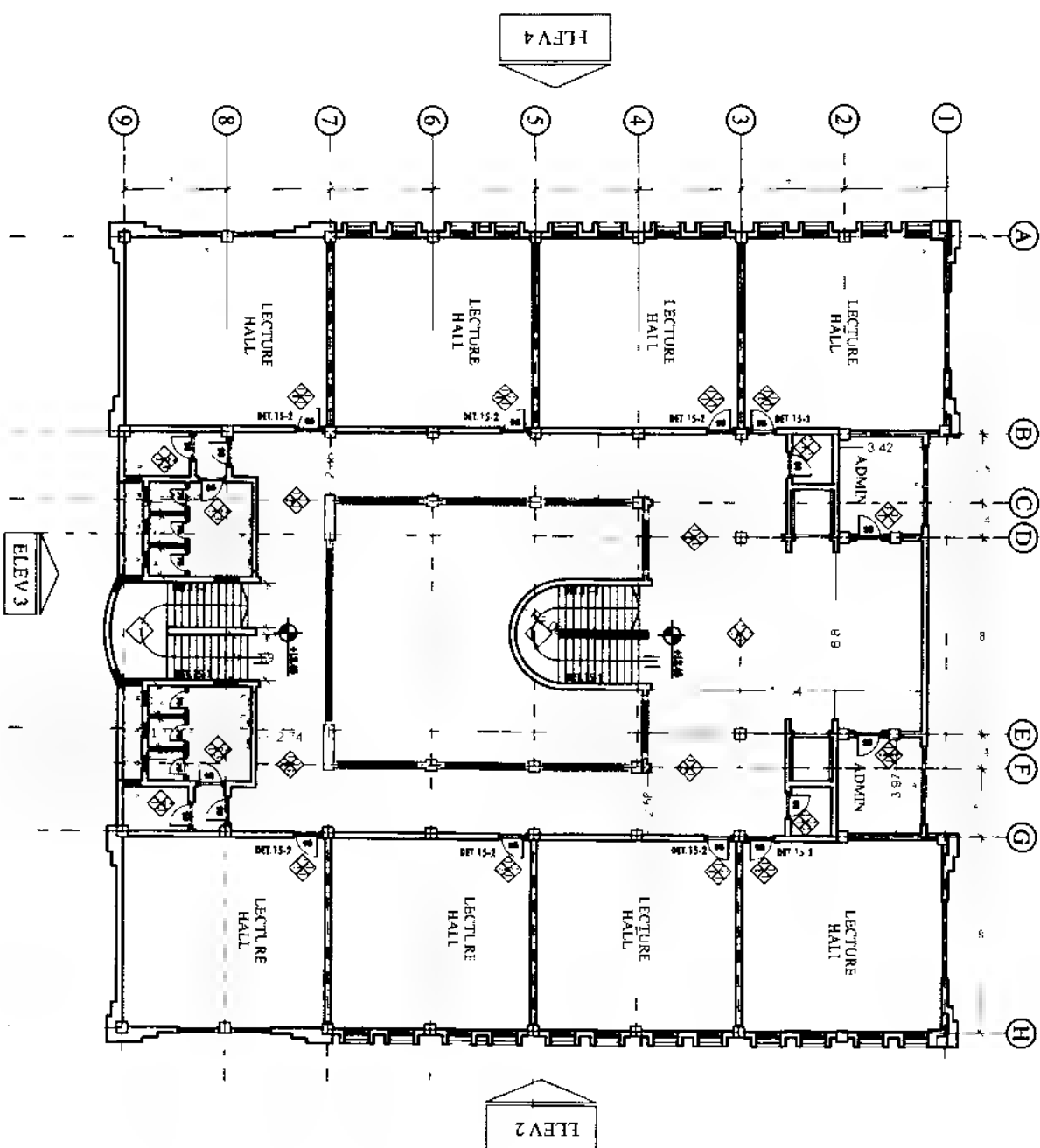
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BUILDING:	
Department Building	
REMARKS:	
FIRST FLOOR PLAN	
CONTRACTOR:	
Scientific & Engineering Consultants Private	
UNIVERSITY OF TECHNOLOGY	
PROJECT NO.:	
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AS:	





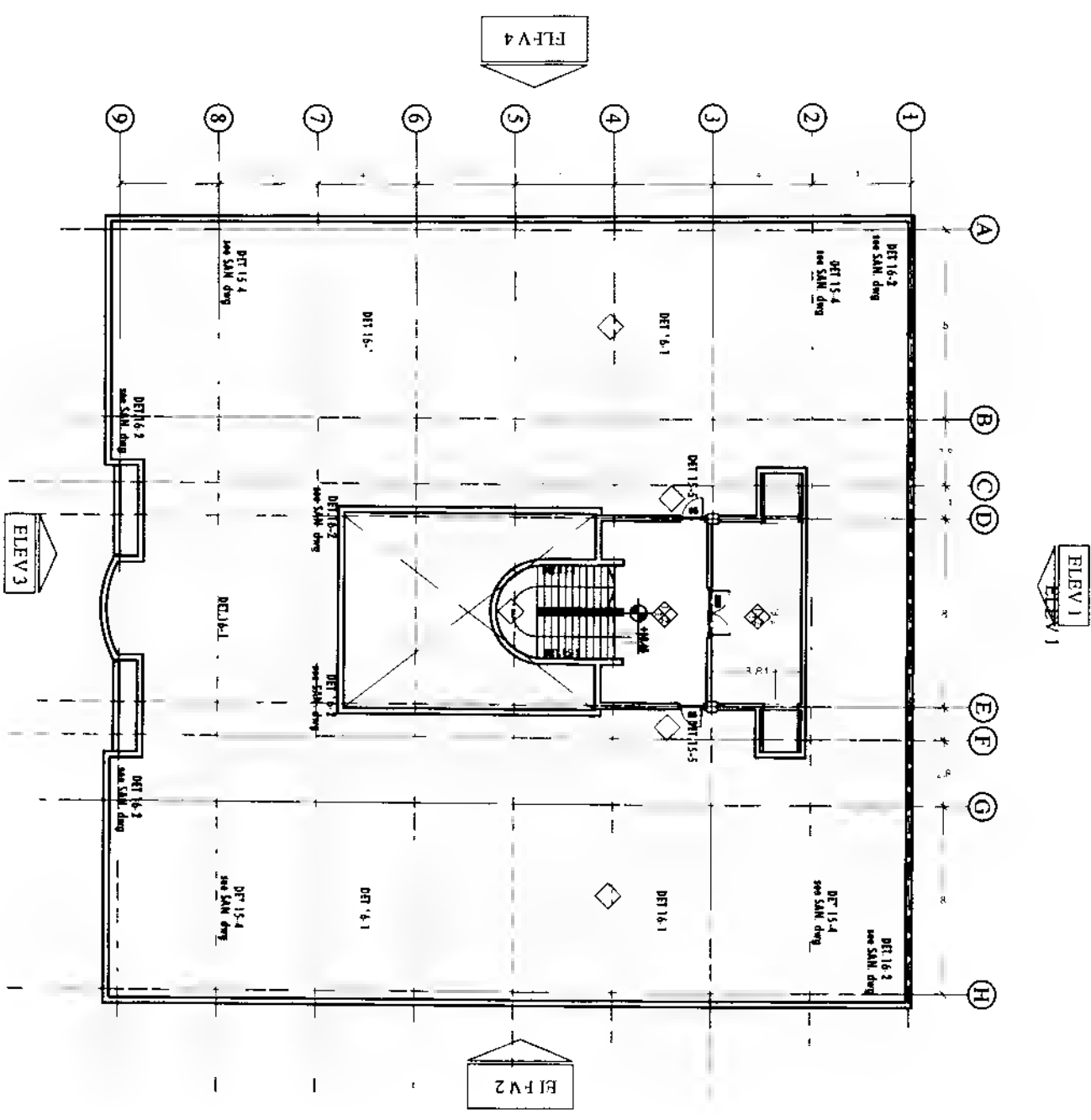
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Department Building			
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CONTRACT			
Scientific & Engineering Community Building			
UNIVERSITY OF TECHNOLOGY			
DESIGNER: R. V.			
DATE	NO.	REV.	REV. NO.
10/10/01	101	101	101



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Department Building			
DRAWING TITLE:			
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CONSULTANT:			
Scientific & Engineering Consultants Bureau			
UNIVERSITY OF TECHNOLOGY			
DRAWING NO.:			
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CHECKED BY:			
SCALE:			
AS SHOWN			



Notes:-

<p><b>QUANTITY</b></p> <p>Scientific &amp; Engineering Consulting Bureau</p> <p>UNIVERSITY OF TECHNOLOGY</p> <p>INTERIOR DIV.</p>			
<p><b>REMARKS</b></p> <p>Department Building</p>			
<p><b>REVISION</b></p> <p>NO. 1</p>			
<p><b>DATE</b></p> <p>1/1/1970</p>			
<p><b>BY</b></p> <p>AS</p>			

ELEV 1

4 ELE

ELEV 3

**ROOM PLAN**

Department Building

**PLAYERS TIME!**

## CONCLUSION

**PERMANENT:**

**अभिज्ञा :**

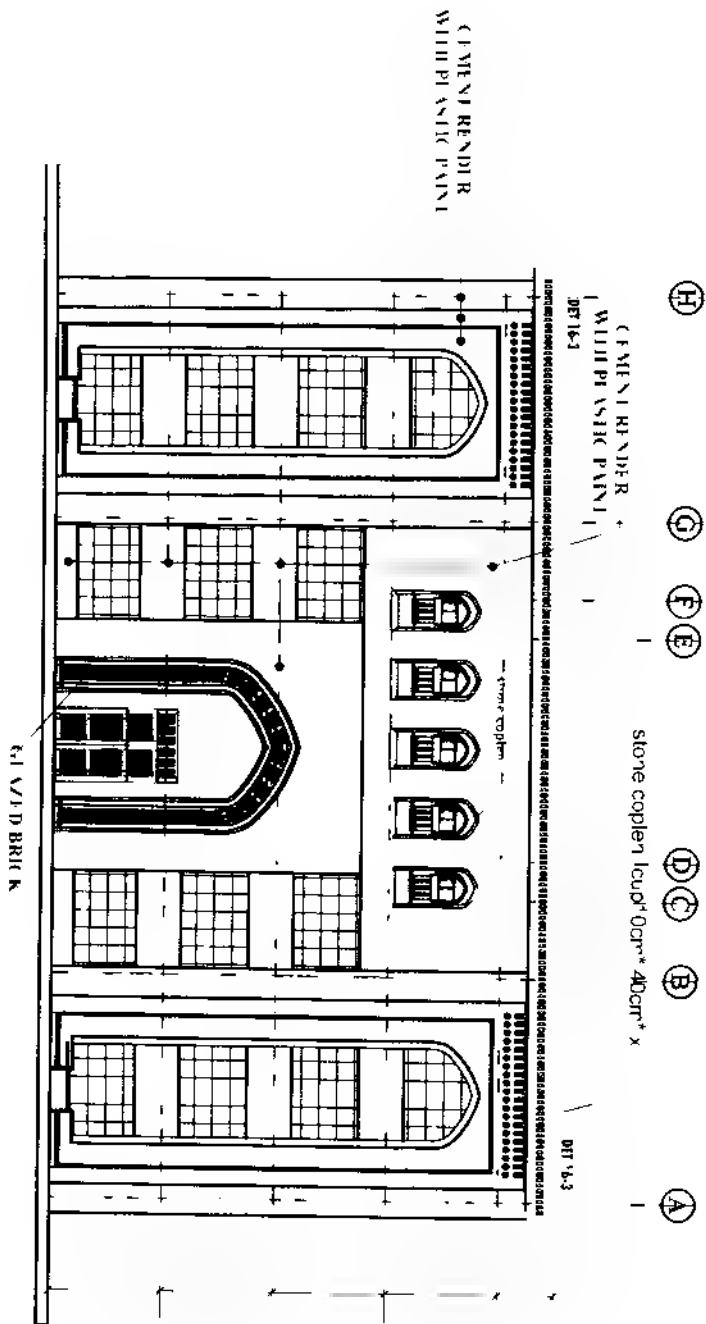
UNIVERSITY OF TECHNOLOGY  
Scientific & Engineering Publications

**PRODUCED BY :**

NAME	ADDRESS	CITY	STATE	ZIP
AL				

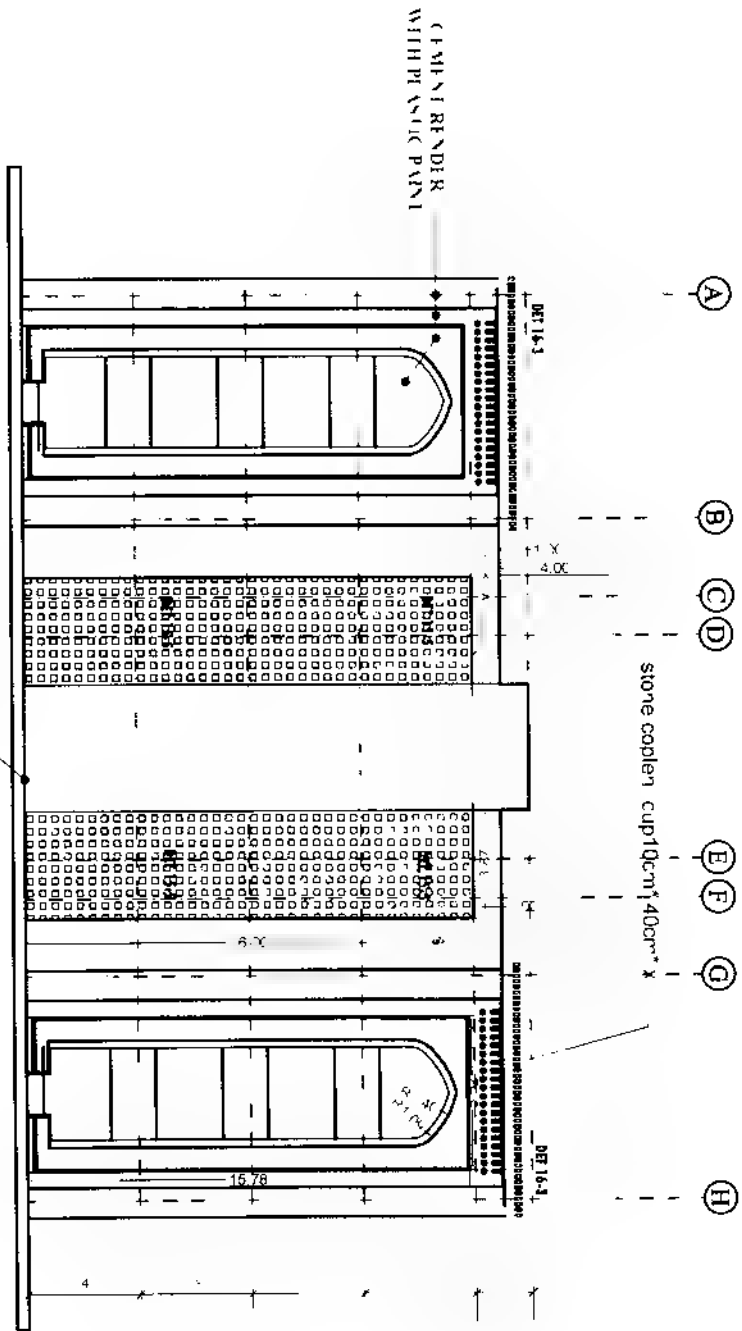
**RESEARCH**

Notes:-



CLIENT			
PROJECT			
DESCRIPTION			
Department Building			
DRAWING TITLE:			
ELEV-1			
CONTRACTOR:			
Scientific & Engineering Consultants Building			
UNIVERSITY OF TECHNOLOGY			
DRAWING BY:			
DATE			
10/10/2023	10/10/2023	10/10/2023	10/10/2023
AS	AS	AS	AS

Notes:-



CLIENT			
PROJECT			
DRAWING			
Department Building			
DRAWING TITLE			
DRAWING NO.			
CONSULTANT			
Scientific & Engineering Consultants Bureau			
UNIVERSITY OF TECHNOLOGY			
REGISTERED NO.			
DATE	BY	CHECKED	APPROVED
1/1/2000	AK		

## ٢-٣ ابعاد المقاطع الإنشائية

### • الأعمدة column

تم اختيار مقاطع الأعمدة حسب المخططات المعمارية وكانت الأبعاد كالآتي

١.  $0.45 \times 1.85$

٢.  $0.45 \times 1.00$

٣.  $0.45 \times 0.45$

### • الرافعات beams

$h = (L \times (0.4 + F_y/700)) / 18.5$  one edge con.

$= (8 \times (0.4 + 420/700)) / 18.5$

$= 0.432 \text{ m}$

$h = (L \times (0.4 + F_y/700)) / 21$  two edge con.

$= (10.8 \times (0.4 + 420/700)) / 21$

$= 0.514 \text{ m}$

Use  $h = 0.6$

Dim. Of beam  $= 0.6 \times 0.3$

لكن في مناطق أخرى كان torsion عالي ولم يتحمل المقطع مما أدى إلى زيادة أبعاد المقطع وأصبح  $(0.8 \times 0.5) \text{ m}$ .

## ● سماك السقف

$$h = (\text{max parameter}/180) \geq 90$$

$$= ((10000 + 4200) * 2) / 180$$

$$= 157.77 \text{ mm}$$

Use h slab = 160 mm

## ٢-٣ التحميل loading

### ● الاحمال الميتة

#### ❖ الحمل الذاتي self weight

و يتم حسابة بالاعتماد على الابعاد السابقة

#### ❖ احمال الارضيات

$$\text{Plate load} = (24 * 0.08 + 0.33) = 2.25 \text{ Kn/m}^2$$

#### ❖ احمال السطح

$$\text{Plate load} = (24 * 0.05 + 18 * 0.13 + 0.3 + 0.3)$$

$$= 4.14 \text{ Kn/m}^2$$

#### ❖ احمال الجدران

$$\text{Member load} = 18 * 0.24 * 4 = 17.24 \text{ kn/m}$$

#### ❖ احمال القواطع الغير مستندة الى beam

$$\text{Plate load} = (18 * 0.24 * 4 * 2.25) / 16 = 2.5 \text{ kn/m}^2$$



## • الإحمال الحية live load

- ❖ الممرات والدرج  $5 \text{ kn/m}^2$
- ❖ الغرف الدراسية  $2 \text{ kn /m}^2$
- ❖ السطح  $1.5 \text{ kn/m}^2$

## • إحمال الرياح wind load

هنا اهتمنا بتأثير حمل الرياح لانه ارتفاع البناية  $16.5\text{m}$  و المواصفة تشترط ان يكون ارتفاع البناية  $19\text{m}$  حتى يدخل تأثير wind load.

## ٣-٤ طريقة الإدخال

- بعد تشغيل البرنامج تظهر الشاشة ادناه والتي يتم من خلالها تعيين نوعية المنشأ وكذلك وحدة القياس الطول والقوة

اختيار نوعية المنشأ

ادخال وحدة الطول

ادخال وحدة القوة

File Name :  
PORTAL

Location  
C:\Users\...

☐ Space  
☒ Portal  
☐ Floor  
☐ Truss

A PLANT structure is defined by a global X-Y coordinate system with loads in the same plane.

Length Units  
☐ Inch  
☒ Foot  
☐ Millimeter  
☐ Centimeter  
☐ Decimeter  
☐ Meter  
☐ Kilometer

Force Units  
☐ Pound  
☐ KiloPound  
☐ Metric Ton  
☐ Newton  
☐ DecaNewton  
☐ KiloNewton  
☐ MegaNewton

☒ Display this dialog box at the Startup

Back Next > Cancel Help

- بعد ذلك تظهر النافذة التالية التي تتم من خلالها عملية الاضافة

تظهر انواع الاختيارات

Welcome to your new project

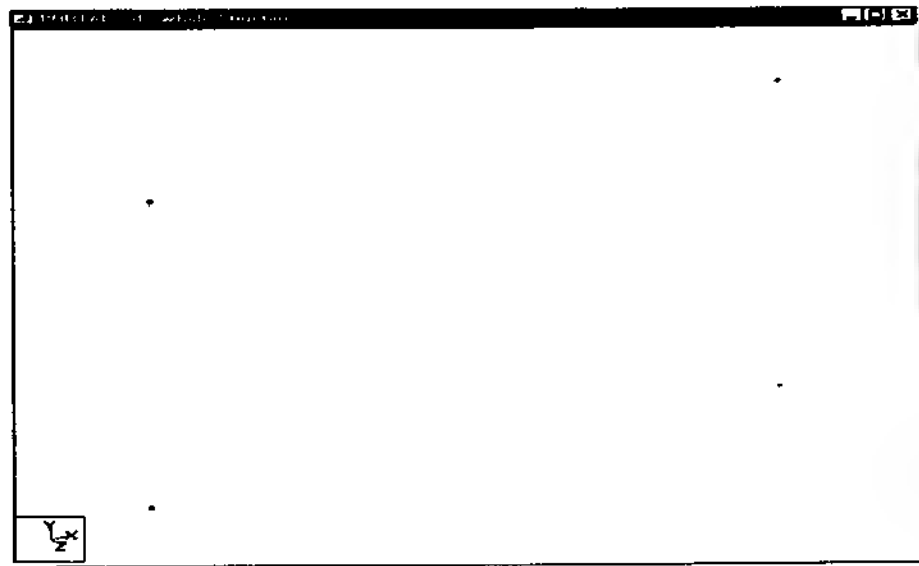
☐ Add Plate  
☐ Add Solid  
☐ Open Structure Wizard  
☐ Open STAAD Editor  
☐ Edit Job Information

Begin building your model by creating new joints and beams using the construction grid, drawing tools and speeddraws.

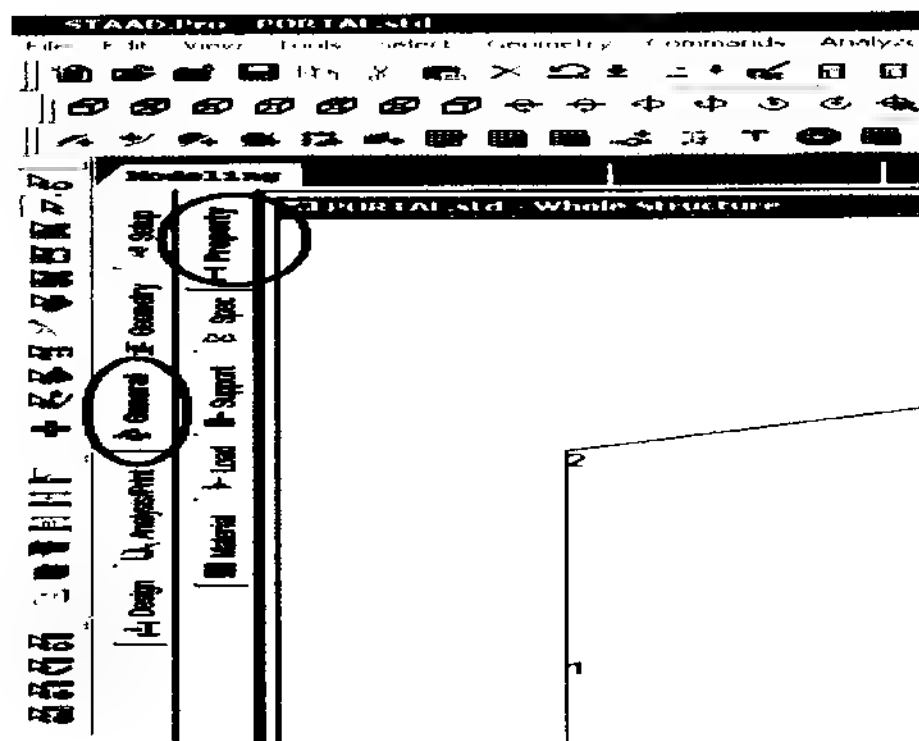
☒ Display this dialog box at the Startup

< Back Finish Cancel Help

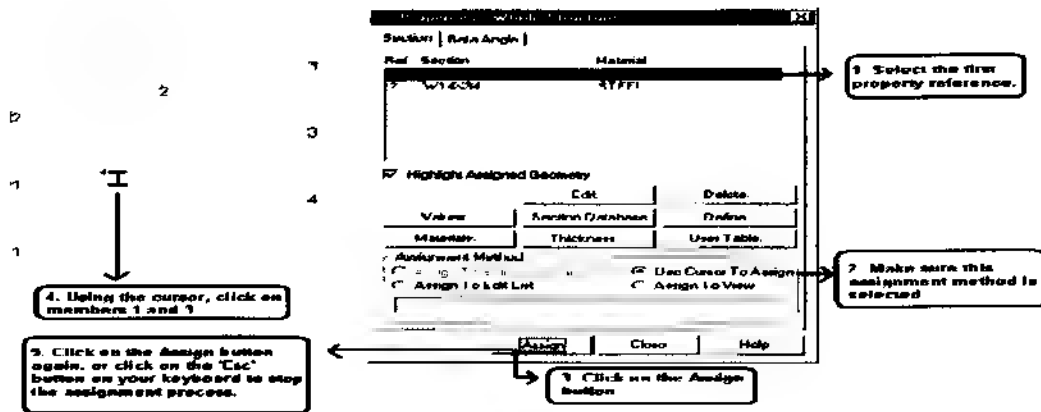
- سنأخذ هذا المثال البسيط لبيان عملية modeling



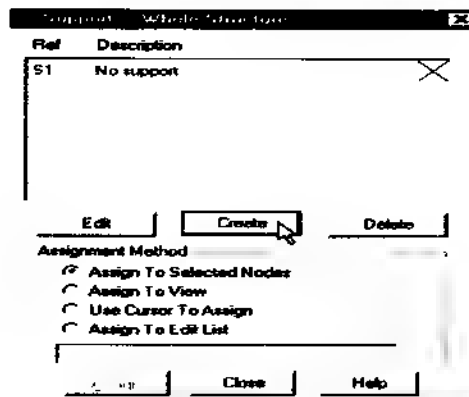
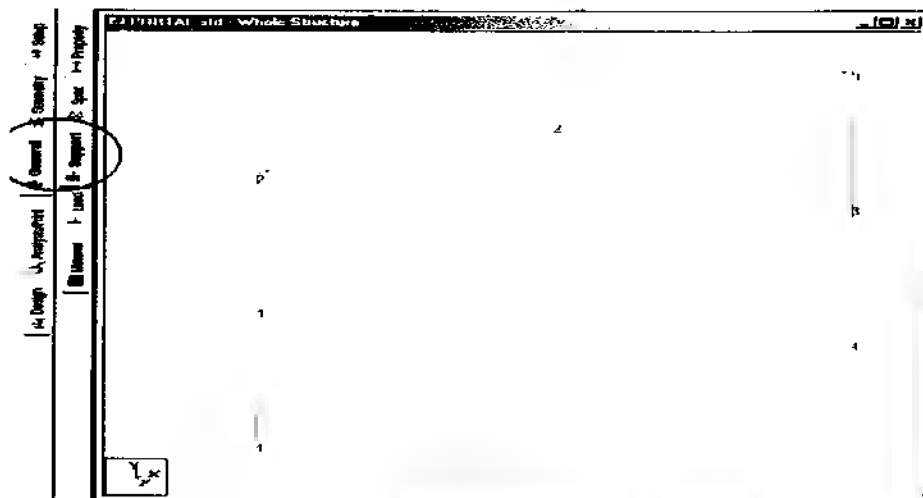
- نبدأ عملية ال modeling بإدخال خصائص المقاطع



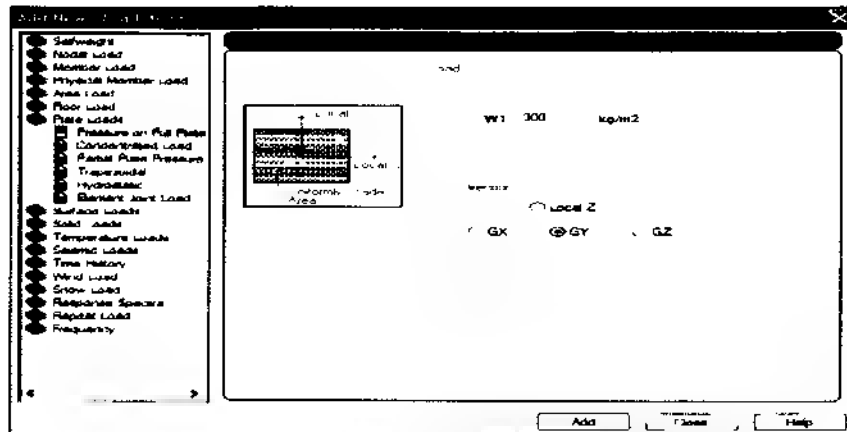
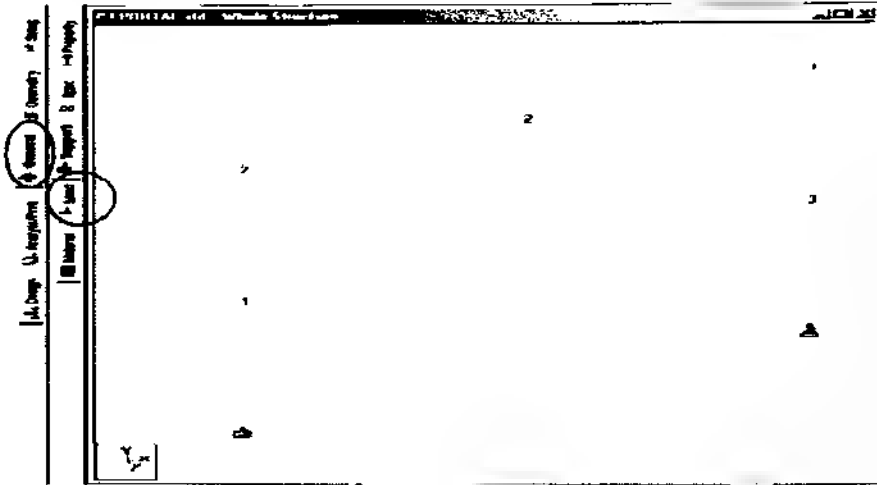
- هذا مثال يبين كيفية اختيار المقاطع وكذلك تخصيصها



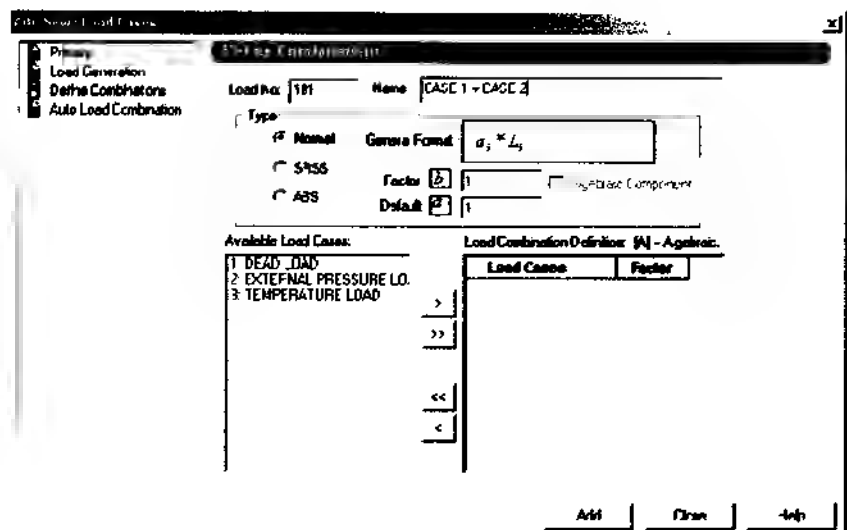
- نبدأ بالمرحلة الثانية وهي ادخال support



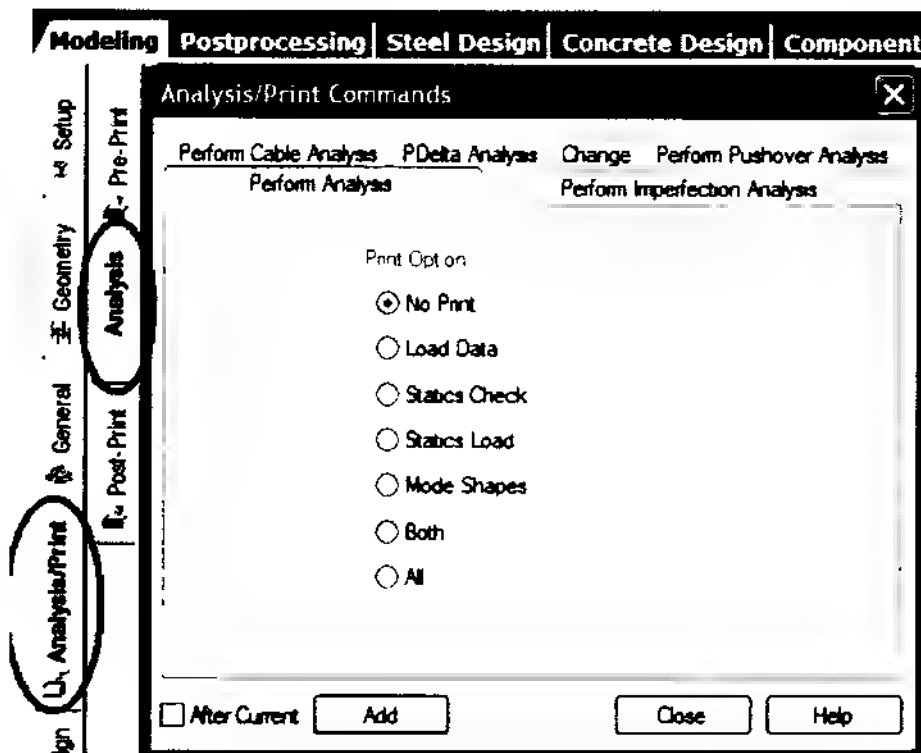
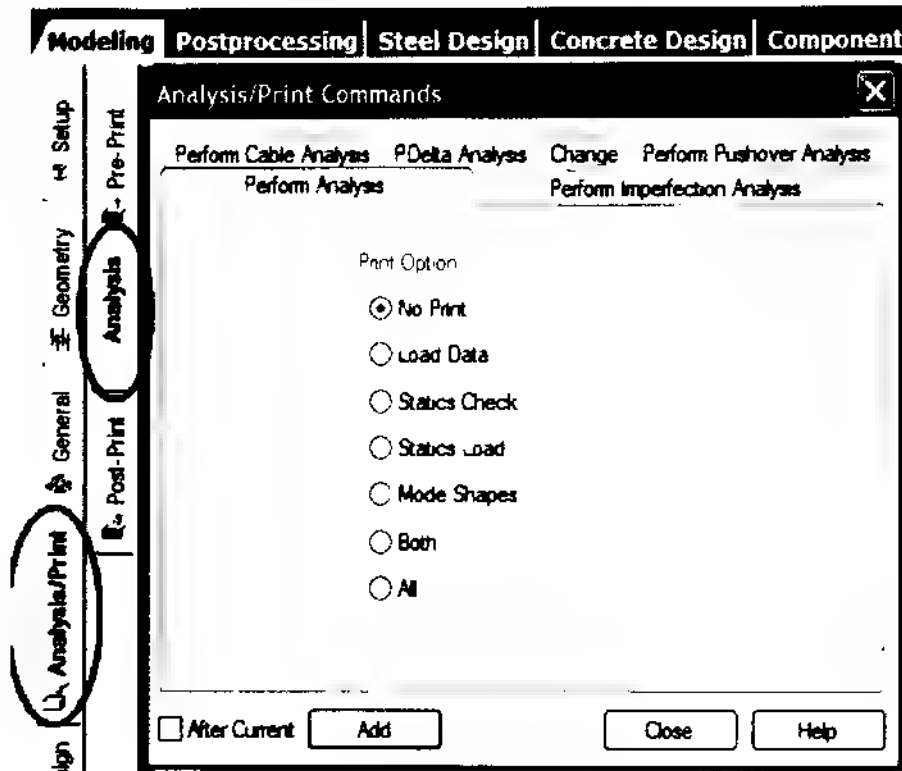
• نبدأ بالمرحلة الثالثة وهي ادخال load



• في بعض الاحيان نعمل load combination لتمثيل الواقع



• بعد الانتهاء من عملية modeling نبدأ بمرحلة Analysis





ملف الأستاذ



PAGE NO.

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*          Proprietary Program of
*          Research Engineers, Intl
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013. 3781 0.4 15.4; 3782 0.4 16.1; 3783 1.666667 4 17.5; 3784 1.666667 4 18.2
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019. 3804 0.4 18.2; 3805 1.666667 4 18.9; 3806 0.833333 4 18.9; 3807 1.666667 4 19.6
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032. 3853 0.4 21.7; 3854 0.4 22.4; 3855 1.666667 4 23.8; 3856 6.333333 4 23.8
033. 3857 5.5 4 23.8; 3858 1.666667 4 24.5; 3859 6.333333 4 24.5; 3860 5.5 4 24.5
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035. 3865 2.5 4 23.8; 3866 4.5 4 24.5; 3867 3.5 4 24.5; 3868 2.5 4 24.5
036. 3869 4.5 4 25.2; 3870 3.5 4 25.2; 3871 1.666667 4 23.8; 3872 0.833333 4 23.8
037. 3873 0.4 23.8; 3874 1.666667 4 24.5; 3875 0.833333 4 24.5; 3876 0.4 24.5
038. 3877 1.666667 4 25.2; 3878 0.833333 4 25.2; 3879 1.666667 4 25.9
039. 3880 1.666667 4 26.6; 3881 1.666667 4 27.3; 3882 6.333333 4 25.9
040. 3883 6.333333 4 26.6; 3884 6.333333 4 27.3; 3885 5.5 4 25.9; 3886 5.5 4 26.6
041. 3887 4.5 4 25.9; 3888 3.5 4 25.9; 3889 2.5 4 25.9; 3890 4.5 4 26.6
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043. 3895 1.666667 4 25.9; 3896 0.833333 4 25.9; 3897 0.4 25.9; 3898 1.666667 4 26.6
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046. 3907 6.333333 4 28.7; 3908 6.333333 4 29.4; 3909 5.5 4 28; 3910 5.5 4 28.7
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STAAD SPACE

-- PAGE NO 20

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# الفصل الأول مختصر التاريخ



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Job No	Sheet No <b>1</b>	Rev
Part		
Ref		
By yasir w.j	Date 05-Dec-10	Chd Dr alaa k.
File design2.std	Date/Time 10-May-2011 09:36	

Job Title building department

Client university of technology

## Job Information

	Engineer	Checked	Approved
Name:	yasir w.j	Dr alaa k	
Date:	05-Dec-10		

Structure Type SPACE FRAME

Number of Nodes	9202	Highest Node	9202
Number of Elements	2879	Highest Beam	11518
Number of Plates	8839	Highest Plate	11494

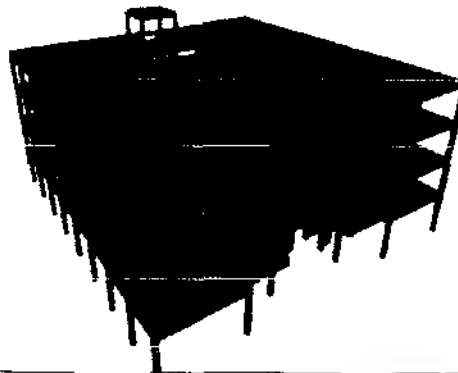
Number of Basic Load Cases	3
Number of Combination Load Cases	3

Included in this printout are data for


All	The Whole Structure
-----	---------------------

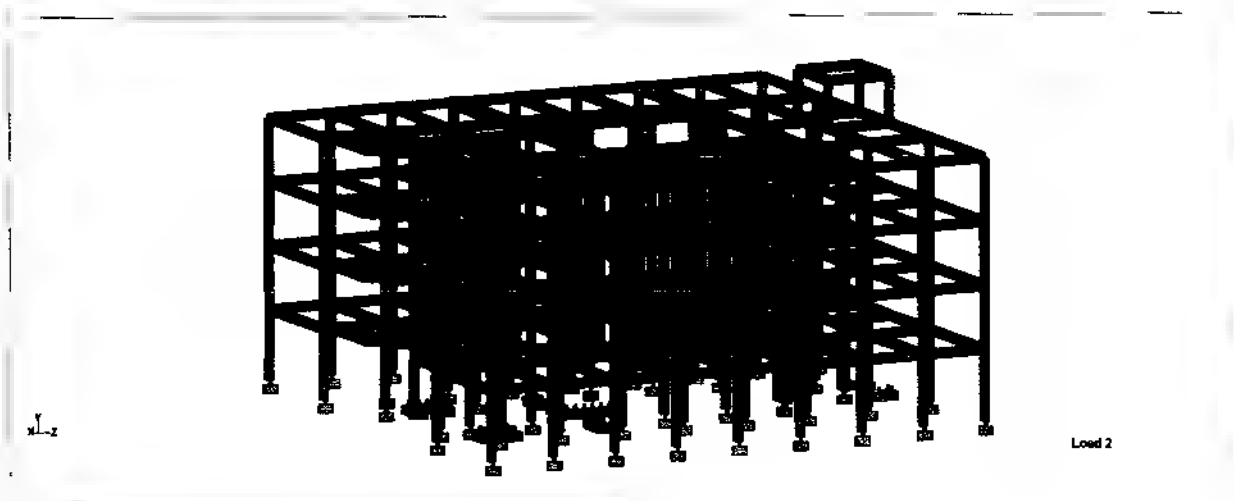
Included in this printout are results for load cases

Type	L/C	Name
Primary	1	DEAD
Primary	2	SELF
Primary	3	LIVE
Combination	4	COMBINATION LOAD CASE 4
Combination	5	COMBINATION LOAD CASE 5
Combination	6	COMBINATION LOAD CASE 6



3D Rendered View

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	Part		
Job Title building department	Ref		
	By yasir w.j	Date 05-Dec-10	Chd Dr alaa k
Client university of technology	File design2.std	Date/Time 10-May-2011 09:36	



Whole Structure

### Section Properties

Prop	Section	Area (cm <sup>2</sup> )	I <sub>yy</sub> (cm <sup>4</sup> )	I <sub>zz</sub> (cm <sup>4</sup> )	J (cm <sup>4</sup> )	Material
7	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
8	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
9	Rect 0.80x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
10	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
11	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
12	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
13	Rect 0.80x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
14	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
15	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
16	Rect 0.80x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
17	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
18	Rect 0.60x0.30	1.8E+3	135E+3	540E+3	371E+3	CONCRETE
19	Rect 0.45x0.45	2.02E+3	342E+3	342E+3	577E+3	CONCRETE
20	Rect 0.80x0.50	4E+3	833E+3	2.13E+6	2.04E+6	CONCRETE
21	Rect 0.80x0.50	4E+3	833E+3	2.13E+6	2.04E+6	CONCRETE
22	Rect 1.00x0.45	4.5E+3	759E+3	3.75E+6	2.18E+6	CONCRETE
23	Rect 1.85x0.45	8.32E+3	1.4E+6	23.7E+6	4.76E+6	CONCRETE



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Job No	Sheet No <b>3</b>	Rev
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Job Title building department

Client university of technology

**Plate Thickness**

Prop	Node A (cm)	Node B (cm)	Node C (cm)	Node D (cm)	Material
1	24.000	24.000	24.000	24.000	CONCRETE
2	45.000	45.000	45.000	45.000	CONCRETE
3	16.000	16.000	16.000	16.000	CONCRETE
4	16.000	16.000	16.000	16.000	CONCRETE
5	16.000	16.000	16.000	16.000	CONCRETE
6	16.000	16.000	16.000	16.000	CONCRETE

**Materials**

Mat	Name	E (kN/mm <sup>2</sup> )	v	Density (kg/m <sup>3</sup> )	$\alpha$ (1/ <sup>o</sup> K)
1	STEEL	205.000	0.300	7.83E+3	12E-6
2	STAINLESSSTEEL	197.930	0.300	7.83E+3	18E-6
3	ALUMINUM	68.948	0.330	2.71E+3	23E-6
4	CONCRETE	21.718	0.170	2.4E+3	10E-6

**Supports**

Node	X (kN/mm)	Y (kN/mm)	Z (kN/mm)	rX (kN/m/deg)	rY (kN/m/deg)	rZ (kN/m/deg)
73	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
74	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
75	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
76	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
77	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
78	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
79	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
80	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
81	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
82	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
83	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
84	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
85	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
86	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
87	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
88	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
89	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
90	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
91	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
92	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
93	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
94	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
95	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
96	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed





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Job No	Sheet No <b>4</b>	Rev
Part		
Ref		
By yasir w.j	Date 05-Dec-10	Chd Dr alaa k.
File design2 std	Date/Time 10-May-2011 09:36	

Job Title building department

Client university of technology

### Supports Cont...

Node	X (kN/mm)	Y (kN/mm)	Z (kN/mm)	rX (kN m/deg)	rY (kN m/deg)	rZ (kN m/deg)
87	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
98	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
99	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
100	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
101	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
102	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
103	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
104	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
105	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
106	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
107	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
108	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
109	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
110	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
111	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
112	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
113	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
114	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
115	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
116	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
117	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
118	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
119	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
120	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
121	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
122	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
123	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
124	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
125	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
126	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
127	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
128	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
129	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
130	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
131	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
132	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
133	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
140	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
143	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
150	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
164	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
165	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
166	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
167	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
168	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
169	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
176	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
243	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed

 Software licensed to Hewlett-Packard	Job No	Sheet No <b>5</b>	Rev
	Part		
Job Title bluiding department	Ref		
	By yasir w j	Date 05-Dec-10	Chd Dr alaa k.
Client university of tecnology	File design2.std	Date/Time 10-May-2011 09:36	

### Supports Cont...

Node	X (kN/mm)	Y (kN/mm)	Z (kN/mm)	rX (kN/m/deg)	rY (kN/m/deg)	rZ (kN/m/deg)
244	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
245	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
246	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
447	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
740	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
1295	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6558	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6565	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6697	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6698	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6787	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6801	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7073	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7074	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7081	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7085	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7106	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7107	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7315	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7320	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7321	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7322	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7422	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7423	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7595	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7599	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7724	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7737	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7748	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7755	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7756	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7922	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
9200	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
9201	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
9202	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed

### Basic Load Cases

Number	Name
2	SELF
3	LIVE
1	DEAD



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## Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
4	COMBINATION LOAD CASE 4	2	SELF	1.00
		3	LIVE	1.00
		1	DEAD	1.00
5	COMBINATION LOAD CASE 5	2	SELF	1.20
		1	DEAD	1.20
		3	LIVE	1.60
6	COMBINATION LOAD CASE 6	2	SELF	1.40
		1	DEAD	1.40


## Node Displacement Summary

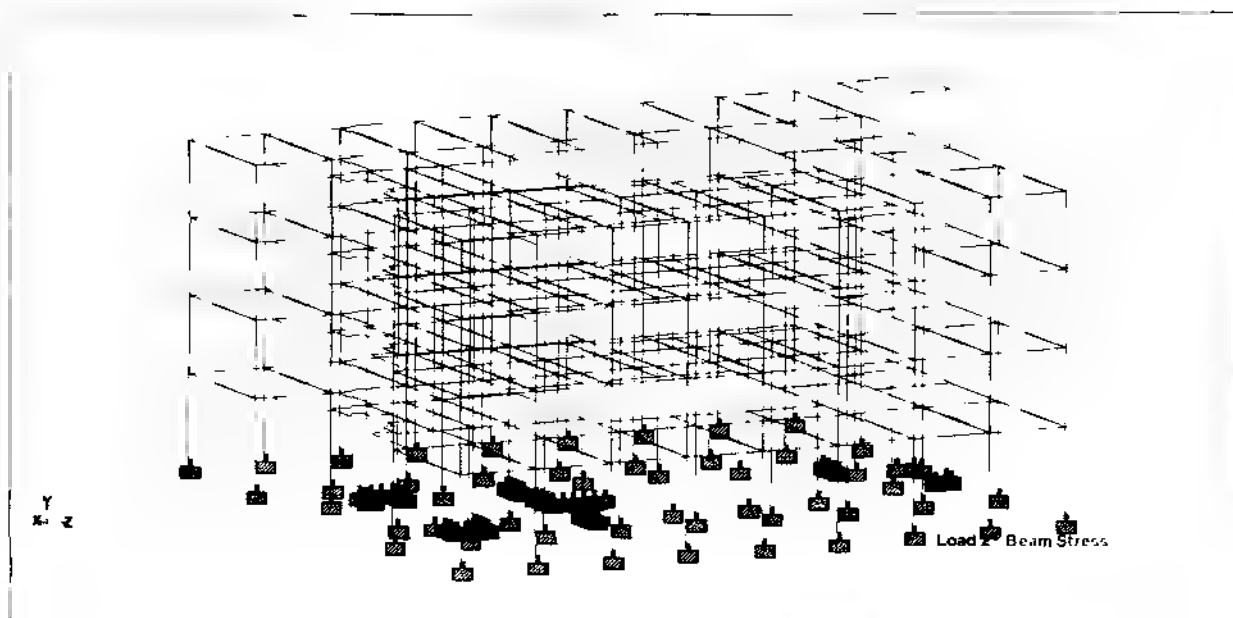
	Node	L/C	X (mm)	Y (mm)	Z (mm)	Resultant (mm)	rX (rad)	rY (rad)	rZ (rad)
Max X	1281	5 COMBINATIK	5.889	-2.498	-0.385	6.390	0.001	0.001	0.000
Min X	137	5 COMBINATIK	-0.725	-2.306	0.196	2.425	0.001	-0.000	0.000
Max Y	73	1 DEAD	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Min Y	6059	6 COMBINATIK	-0.147	-14.837	-1.168	14.883	0.000	-0.000	-0.001
Max Z	1282	5 COMBINATIK	4.418	-3.783	1.209	5.940	-0.001	0.001	0.001
Min Z	7898	5 COMBINATIK	-0.139	-4.313	-3.312	5.440	-0.000	-0.000	-0.000
Max rX	8911	5 COMBINATIK	-0.259	-4.574	-0.680	4.831	0.003	-0.000	-0.001
Min rX	6310	5 COMBINATIK	-0.229	-4.369	-1.121	4.517	-0.004	0.000	-0.000
Max rY	7383	5 COMBINATIK	3.834	-1.333	-0.483	4.087	-0.000	0.001	0.001
Min rY	7211	5 COMBINATIK	0.645	-5.954	-0.308	5.996	-0.001	-0.001	0.002
Max rZ	6438	6 COMBINATIK	-0.295	-7.341	-1.168	7.438	0.000	0.000	0.004
Min rZ	8084	6 COMBINATIK	-0.137	-7.371	1.171	7.465	0.000	-0.000	-0.004
Max Rst	6059	6 COMBINATIK	-0.147	-14.837	-1.168	14.883	0.000	-0.000	-0.001

## Beam Displacement Detail Summary

Displacements shown in *italic* indicate the presence of an offset

	Beam	L/C	d (m)	X (mm)	Y (mm)	Z (mm)	Resultant (mm)
Max X	8320	5 COMBINATIK	1.350	1.219	-1.172	-0.062	1.693
Min X	104	6 COMBINATIK	1.200	-1.484	-3.880	-1.063	4.281
Max Y	21	1 DEAD	4.500	0.000	0.000	0.000	0.000
Min Y	427	6 COMBINATIK	0.600	-0.154	-13.948	-1.168	13.998
Max Z	2160	5 COMBINATIK	1.350	-0.039	-0.772	0.451	0.895
Min Z	2168	5 COMBINATIK	0.105	-0.139	-4.304	-3.312	5.433
Max Rst	427	6 COMBINATIK	0.600	-0.154	-13.948	-1.168	13.998

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Whole Structure Beam Stress 5e+007mm.m 2 SELF

## Beam End Force Summary

The signs of the forces at end B of each beam have been reversed For example this means that the Min Fx entry gives the largest tension value for an beam

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kN)	Fy (kN)	Fz (kN)	Mx (kNm)	My (kNm)	Mz (kNm)
Max Fx	2875	108	5 COMBINATIC	2.83E+3	27 725	-12.030	-0.508	-20.379	8.481
Min Fx	2537	56	5 COMBINATIC	-120.060	-442 560	-19 905	-21 938	7.668	34.094
Max Fy	1888	6159	8 COMBINATIC	-31 703	481.203	-1 257	54 086	-0.060	293.304
Min Fy	2537	128	5 COMBINATIC	-120 060	-456.184	-19 905	-21.938	-0.808	225.436
Max Fz	2186	1052	5 COMBINATIC	499 085	24 863	79.847	-0.660	-169.088	56 722
Min Fz	2839	788	5 COMBINATIC	575 865	22 476	-49.524	0 025	99 855	44.093
Max Mx	1681	6089	6 COMBINATIC	24.559	207 848	-5.479	157.185	0.333	-37 714
Min Mx	3026	1036	6 COMBINATIC	24 623	-191 822	4.801	-158.144	-1 780	-125.104
Max My	2418	812	5 COMBINATIC	483 358	-27 257	79 733	0 064	153.823	42.263
Min My	2186	1052	5 COMBINATIC	499 085	24 863	79.847	-0.660	-169.088	56 722
Max Mz	1930	504	5 COMBINATIC	38 078	312 178	-0 014	-88.269	-1.407	508.231
Min Mz	8148	5428	5 COMBINATIC	35 528	1 353	-0 002	-1.913	-0.009	-407.886



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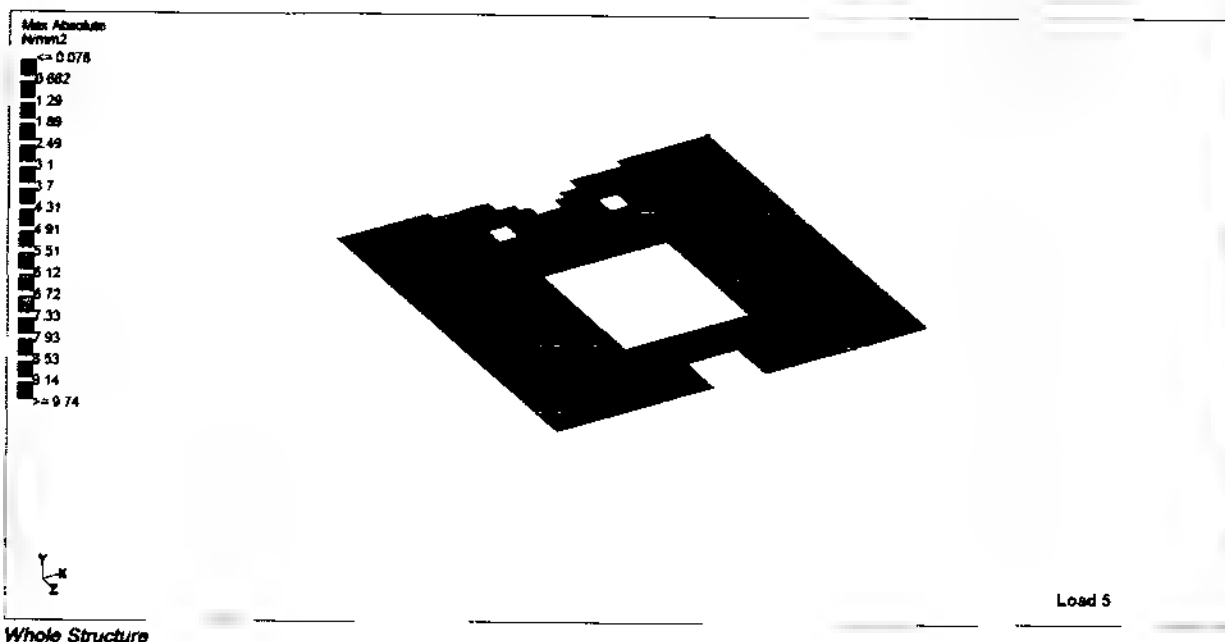
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## Plate Centre Stress Summary

	Plate	LC	Shear		Membrane			Bending		
			Qx (N/mm <sup>2</sup> )	Qy (N/mm <sup>2</sup> )	Sx (N/mm <sup>2</sup> )	Sy (N/mm <sup>2</sup> )	Sxy (N/mm <sup>2</sup> )	Mx (kNm/m)	My (kNm/m)	Mxy (kNm/m)
Max Qx	11137	5-COMBINATK	0.759	0.734	-0.454	-1.307	0.101	31.689	35.890	0.095
Min Qx	11148	5-COMBINATK	-0.739	0.778	0.513	1.174	0.190	32.835	35.836	-0.233
Max Qy	11148	5-COMBINATK	-0.799	0.776	0.513	1.174	0.190	32.835	35.836	-0.233
Min Qy	11485	5-COMBINATK	-0.245	-0.743	-0.014	-0.122	0.024	15.518	6.691	3.808
Max Sx	8844	5-COMBINATK	-0.573	-0.146	2.118	0.405	0.433	25.072	9.368	14.406
Min Sx	9000	5-COMBINATK	0.038	-0.002	-4.715	-0.801	0.462	3.167	0.538	0.284
Max Sy	5548	5-COMBINATK	-0.688	0.697	0.495	1.618	-0.134	28.961	34.489	-0.815
Min Sy	7892	8-COMBINATK	-0.073	0.052	-1.267	-4.929	1.153	-1.058	-6.369	2.643
Max Sxy	8910	5-COMBINATK	-0.044	-0.022	-1.906	-1.011	2.009	-7.640	-4.421	-0.188
Min Sxy	8902	5-COMBINATK	-0.016	-0.017	-2.555	-1.505	-1.909	2.990	0.842	1.597
Max Mx	9248	5-COMBINATK	-0.737	0.494	-0.001	0.695	0.074	75.473	33.318	5.873
Min Mx	8839	5-COMBINATK	0.748	-0.480	-0.062	0.450	-0.046	-79.013	-32.893	-7.258
Max My	9544	5-COMBINATK	0.025	-0.140	-0.743	2.677	1.582	11.039	77.480	-14.097
Min My	9539	5-COMBINATK	-0.022	0.136	-0.358	-1.394	0.777	-10.104	-76.297	12.858
Max Mxy	9510	5-COMBINATK	-0.080	0.138	-0.173	0.112	-0.138	-13.962	-55.445	25.028
Min Mxy	9520	5-COMBINATK	0.069	-0.148	-0.455	0.548	-0.263	17.354	55.523	-28.063



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## Reaction Summary

	Node	L/C	Horizontal FX (kN)	Vertical FY (kN)	Horizontal FZ (kN)	Moment		
						MX (kNm)	MY (kNm)	MZ (kNm)
Max FX	184	6-COMBINATK	112.074	884.328	-73.121	52.509	-1.396	18.671
Min FX	165	6-COMBINATK	-107.818	832.626	-79.660	50.084	1.470	-18.006
Max FY	108	5-COMBINATK	-27.725	2.83E+3	12.030	20.379	-0.508	-8.481
Min FY	166	3-LIVE	1.818	-9.788	-9.530	-4.201	0.180	-0.856
Max FZ	7599	5-COMBINATK	-2.121	87.078	93.938	19.155	7.115	-3.834
Min FZ	165	5-COMBINATK	-97.884	811.395	-81.026	48.331	1.806	-15.527
Max MX	164	6-COMBINATK	112.074	884.328	-73.121	52.509	-1.396	18.671
Min MX	186	6-COMBINATK	1.999	325.347	29.845	-56.244	1.975	-6.771
Max MY	7599	5-COMBINATK	-2.121	87.078	93.938	-19.155	7.115	-3.834
Min MY	114	5-COMBINATK	-0.240	256.216	65.677	-23.893	-5.059	5.317
Max MZ	100	5-COMBINATK	-40.290	1.65E+3	0.480	1.428	-0.012	69.582
Min MZ	111	5-COMBINATK	55.320	2.8E+3	10.646	17.266	1.159	-112.481

## Reactions

Node	L/C	Horizontal FX (kN)	Vertical FY (kN)	Horizontal FZ (kN)	Moment		
					MX (kNm)	MY (kNm)	MZ (kNm)
73	1-DEAD	10.475	653.985	1.038	2.074	0.024	-15.871
	2-SELF	9.919	485.592	-0.040	0.040	0.015	-14.987
	3-LIVE	3.960	119.679	0.008	0.008	0.013	-6.014
	4-COMBINATK	24.354	1.24E+3	1.005	2.122	0.051	-36.852
	5-COMBINATK	30.806	1.53E+3	1.209	2.550	0.067	-46.628
	6-COMBINATK	28.552	1.57E+3	1.396	2.960	0.054	-43.173
74	1-DEAD	8.847	704.897	-0.155	0.291	0.008	-13.407
	2-SELF	9.680	538.882	0.065	0.185	0.008	-14.541
	3-LIVE	3.378	127.447	-0.020	-0.042	0.007	-5.121
	4-COMBINATK	21.884	1.37E+3	-0.111	0.435	0.023	-33.070
	5-COMBINATK	27.612	1.7E+3	-0.141	0.505	0.030	-41.732
	6-COMBINATK	25.909	1.74E+3	-0.127	0.667	0.023	-39.128
75	1-DEAD	16.782	752.941	0.314	0.977	0.000	-25.145
	2-SELF	10.233	468.736	0.097	0.224	-0.001	15.395
	3-LIVE	4.189	121.996	-0.086	-0.146	-0.000	-6.292
	4-COMBINATK	31.185	1.34E+3	0.325	1.054	-0.001	-46.832
	5-COMBINATK	39.085	1.66E+3	0.355	1.205	-0.001	-58.715
	6-COMBINATK	37.793	1.71E+3	0.576	1.682	-0.001	-56.756
76	1-DEAD	11.210	895.325	1.007	2.011	0.004	-16.918
	2-SELF	10.337	467.396	0.009	0.095	-0.003	15.558
	3-LIVE	4.229	121.185	0.023	0.013	-0.003	-6.387
	4-COMBINATK	25.775	1.28E+3	1.040	2.118	-0.002	-38.862
	5-COMBINATK	32.622	1.59E+3	1.257	2.548	-0.004	-49.189
	6-COMBINATK	30.165	1.63E+3	1.423	2.947	0.001	-45.464
77	1-DEAD	9.220	706.107	-0.080	0.416	0.009	-13.961




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**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	2-SELF	10.231	530.644	0.061	0.183	0.001	-15.402
	3-LIVE	3.896	122.833	-0.034	-0.067	-0.002	-5.604
	4-COMBINATK	23.147	1.36E+3	-0.053	0.531	0.008	-34.967
	5-COMBINATK	29.254	1.68E+3	-0.077	0.611	0.008	-44.201
	6-COMBINATK	27.231	1.73E+3	-0.027	0.837	0.013	-41.108
78	1-DEAD	17.781	746.827	0.384	1.113	0.010	-26.569
	2-SELF	10.340	469.295	0.117	0.278	0.003	-15.562
	3-LIVE	4.241	121.357	-0.074	-0.121	-0.001	-6.417
	4-COMBINATK	32.341	1.34E+3	0.427	1.268	0.012	-48.547
	5-COMBINATK	40.506	1.65E+3	0.483	1.474	0.014	-60.823
	6-COMBINATK	39.341	1.7E+3	0.702	1.945	0.019	-58.983
79	1-DEAD	11.501	740.701	0.495	1.282	0.009	-17.307
	2-SELF	10.578	465.397	0.125	0.293	0.003	-15.908
	3-LIVE	4.421	124.448	-0.006	-0.016	-0.001	-6.687
	4-COMBINATK	28.500	1.33E+3	0.614	1.560	0.011	-39.902
	5-COMBINATK	33.568	1.65E+3	0.735	1.866	0.013	-50.557
	6-COMBINATK	30.910	1.69E+3	0.666	2.206	0.017	-46.500
80	1-DEAD	13.687	569.377	3.961	6.417	-0.032	-20.531
	2-SELF	6.772	303.517	2.251	3.444	-0.013	-10.271
	3-LIVE	2.411	60.836	0.833	1.228	-0.006	-3.716
	4-COMBINATK	22.671	933.729	7.045	11.089	-0.050	-34.518
	5-COMBINATK	28.408	1.14E+3	8.788	13.798	-0.063	-42.908
	6-COMBINATK	28.643	1.22E+3	8.697	13.806	-0.062	-43.122
81	1-DEAD	-8.268	815.811	0.044	0.567	0.009	12.044
	2-SELF	-7.410	567.287	-0.141	-0.105	-0.001	10.764
	3-LIVE	-2.975	164.150	-0.032	-0.039	-0.004	4.280
	4-COMBINATK	-18.654	1.55E+3	-0.129	0.424	0.004	27.089
	5-COMBINATK	-23.575	1.92E+3	-0.168	0.494	0.004	34.218
	6-COMBINATK	-21.950	1.94E+3	-0.136	0.648	0.012	31.931
82	1-DEAD	-10.523	927.928	0.957	1.914	0.014	15.345
	2-SELF	-6.184	630.519	0.648	1.055	0.003	8.941
	3-LIVE	-1.983	222.054	0.732	1.088	-0.002	2.810
	4-COMBINATK	-18.689	1.78E+3	2.335	4.057	0.015	27.096
	5-COMBINATK	-23.220	2.23E+3	3.095	5.303	0.017	33.639
	6-COMBINATK	-23.389	2.18E+3	2.244	4.157	0.024	34.000
83	1-DEAD	-6.468	922.289	-0.018	0.470	0.009	9.271
	2-SELF	-6.412	763.792	-0.005	0.083	-0.000	9.240
	3-LIVE	-1.950	281.765	-0.208	-0.314	-0.003	2.751
	4-COMBINATK	-14.828	1.99E+3	-0.230	0.000	0.006	21.262
	5-COMBINATK	-18.573	2.5E+3	-0.358	0.161	0.006	26.615
	6-COMBINATK	-18.029	2.39E+3	-0.032	0.774	0.013	25.916
84	1-DEAD	-8.862	807.282	0.762	1.611	-0.001	9.870
	2-SELF	-8.287	618.936	-0.203	-0.226	-0.004	9.053
	3-LIVE	-2.051	232.176	-0.038	-0.078	-0.003	2.921

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## Reactions Cont...

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	4-COMBINATK	-15.179	1.66E+3	0.521	1.307	-0.008	21.844
	5-COMBINATK	-19.036	2.08E+3	0.610	1.537	-0.011	27.381
	6-COMBINATK	-18.380	1.99E+3	0.783	1.938	-0.007	26.492
85	1-DEAD	-5.538	763.850	0.239	0.811	0.013	7.925
	2-SELF	-5.650	680.838	0.321	0.515	0.011	6.157
	3-LIVE	-1.548	231.058	0.318	0.418	0.009	2.184
	4-COMBINATK	-12.736	1.66E+3	0.879	1.745	0.033	18.267
	5-COMBINATK	-15.902	2.1E+3	1.182	2.261	0.044	22.794
	6-COMBINATK	-15.663	2.02E+3	0.785	1.858	0.033	22.516
86	1-DEAD	-10.804	850.452	0.109	0.634	0.002	15.721
	2-SELF	-6.284	601.795	0.013	0.077	-0.000	9.096
	3-LIVE	-2.065	224.980	-0.186	-0.311	0.001	2.953
	4-COMBINATK	-19.153	1.68E+3	-0.064	0.400	0.002	27.770
	5-COMBINATK	-23.810	2.1E+3	-0.151	0.355	0.003	34.505
	6-COMBINATK	-23.923	2.03E+3	0.171	0.996	0.002	34.744
87	1-DEAD	-1.042	993.379	1.596	2.609	0.024	1.230
	2-SELF	3.598	712.806	-0.000	0.027	0.023	5.090
	3-LIVE	-0.133	268.404	-0.860	-1.041	0.018	0.068
	4-COMBINATK	-4.771	1.97E+3	0.936	1.795	0.066	6.367
	5-COMBINATK	-5.778	2.48E+3	0.859	1.738	0.086	7.692
	6-COMBINATK	-6.493	2.39E+3	2.234	3.971	0.066	8.847
88	1-DEAD	-5.202	874.162	-4.628	-6.413	0.015	7.308
	2-SELF	2.550	456.287	-3.425	-5.049	0.021	3.457
	3-LIVE	-0.778	110.307	-1.559	-2.375	0.020	0.954
	4-COMBINATK	-8.528	1.44E+3	-9.612	-13.837	0.056	11.720
	5-COMBINATK	-10.544	1.77E+3	-12.158	17.555	0.076	14.446
	6-COMBINATK	-10.852	1.88E+3	-11.275	-16.047	0.051	15.072
89	1-DEAD	5.052	895.071	-4.769	-6.666	0.006	-7.659
	2-SELF	2.736	485.176	-3.446	-5.033	0.003	-4.214
	3-LIVE	0.965	113.395	-1.557	-2.327	-0.003	-1.514
	4-COMBINATK	8.753	1.47E+3	-9.773	-14.026	0.006	-13.387
	5-COMBINATK	10.889	1.81E+3	-12.350	-17.762	0.006	-16.670
	6-COMBINATK	10.903	1.9E+3	-11.502	-16.378	0.013	-16.623
90	1-DEAD	0.672	1.02E+3	1.856	2.857	-0.000	-1.180
	2-SELF	3.555	724.360	0.122	0.280	0.001	5.420
	3-LIVE	0.062	274.934	-0.579	-0.872	-0.002	-0.176
	4-COMBINATK	4.289	2.02E+3	1.200	2.245	-0.001	-6.775
	5-COMBINATK	5.171	2.53E+3	1.208	2.345	-0.001	-8.201
	6-COMBINATK	5.917	2.44E+3	2.489	4.363	0.001	-9.240
91	1-DEAD	6.097	781.710	0.242	0.778	0.008	-9.195
	2-SELF	6.105	677.446	0.407	0.696	0.007	-9.184
	3-LIVE	1.795	229.806	0.389	0.572	0.001	-2.741
	4-COMBINATK	13.997	1.67E+3	1.036	2.045	0.016	-21.119
	5-COMBINATK	17.514	2.09E+3	1.401	2.683	0.020	-26.440





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Job No	Sheet No <b>12</b>	Rev
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By yasir w.j	Date 05-Dec-10	Chd Dr alaa k
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**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
92	8:COMBINATK	17.083	2.01E+3	0.908	2.063	0.022	-25.730
	1:DEAD	11.185	849.552	0.064	0.530	0.020	-16.637
	2:SELF	6.580	599.773	0.063	0.198	0.013	-9.848
	3:LIVE	2.242	224.185	-0.141	-0.203	0.004	-3.391
	4:COMBINATK	19.987	1.87E+3	-0.014	0.525	0.037	-29.876
	5:COMBINATK	24.881	2.1E+3	-0.073	1.549	0.046	-37.207
93	6:COMBINATK	24.843	2.03E+3	0.177	1.020	0.046	-37.079
	1:DEAD	7.138	806.956	0.734	1.532	0.022	-10.600
	2:SELF	6.521	815.978	-0.159	-0.122	0.014	9.711
	3:LIVE	2.225	232.181	-0.004	0.008	0.004	-3.351
	4:COMBINATK	15.884	1.66E+3	0.571	1.418	0.040	-23.662
	5:COMBINATK	19.931	2.08E+3	0.684	1.701	0.050	-29.735
94	6:COMBINATK	19.122	1.99E+3	0.806	1.974	0.050	-28.435
	1:DEAD	6.830	921.894	-0.044	0.392	0.008	-10.068
	2:SELF	6.824	787.384	0.045	0.188	0.004	-10.106
	3:LIVE	2.253	225.088	-0.168	-0.228	0.001	-3.373
	4:COMBINATK	15.907	2E+3	-0.167	0.352	0.012	-23.548
	5:COMBINATK	19.890	2.51E+3	-0.288	0.331	0.015	-29.607
95	6:COMBINATK	19.118	2.39E+3	0.001	0.813	0.016	-28.244
	1:DEAD	10.691	928.516	0.907	1.801	-0.006	-15.835
	2:SELF	6.432	830.746	0.688	1.143	-0.006	-9.576
	3:LIVE	2.196	222.391	0.771	1.166	-0.003	-3.319
	4:COMBINATK	19.318	1.78E+3	2.366	4.110	-0.015	-28.730
	5:COMBINATK	24.061	2.23E+3	3.148	5.399	-0.019	-35.803
96	6:COMBINATK	23.971	2.18E+3	2.234	4.122	-0.016	-35.575
	1:DEAD	8.484	824.993	-0.033	0.408	0.003	-12.589
	2:SELF	7.647	587.906	-0.127	-0.063	-0.000	-11.392
	3:LIVE	3.180	162.995	-0.012	0.008	0.000	-4.786
	4:COMBINATK	19.310	1.58E+3	-0.173	0.358	0.002	-28.767
	5:COMBINATK	24.445	1.93E+3	-0.213	0.428	0.003	-36.435
97	6:COMBINATK	22.583	1.95E+3	-0.225	0.484	0.003	-33.573
	1:DEAD	7.545	790.055	5.618	9.081	-0.008	-11.192
	2:SELF	3.322	459.005	3.650	5.534	0.003	-4.991
	3:LIVE	1.538	89.014	1.406	2.110	-0.000	-2.357
	4:COMBINATK	12.405	1.34E+3	10.874	16.724	-0.006	-18.540
	5:COMBINATK	15.501	1.84E+3	13.611	20.913	-0.007	-23.191
98	6:COMBINATK	15.214	1.75E+3	13.255	20.461	-0.008	-22.656
	1:DEAD	-13.703	587.487	3.850	6.153	0.040	20.355
	2:SELF	-8.700	302.973	2.283	3.516	0.010	9.881
	3:LIVE	-2.285	60.708	0.878	1.333	0.002	3.315
	4:COMBINATK	-22.888	931.168	7.011	11.002	0.051	33.552
	5:COMBINATK	-28.138	1.14E+3	8.785	13.736	0.062	41.588
99	6:COMBINATK	-28.584	1.22E+3	8.586	13.537	0.069	42.331
	1:DEAD	-11.528	729.058	0.389	1.024	0.001	17.121



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Job Title building department

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**Reactions Cont...**

Node	LC	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	2:SELF	-10.518	484.711	0.156	0.364	-0.006	15.542
	3:LIVE	-4.307	124.198	0.043	0.095	-0.003	6.317
	4:COMBINATK	-28.351	1.32E+3	0.588	1.483	-0.008	38.979
	5:COMBINATK	-33.344	1.63E+3	0.723	1.817	-0.011	49.302
	6:COMBINATK	-30.882	1.87E+3	0.763	1.944	-0.007	45.728
100	1:DEAD	-17.748	744.590	0.294	0.874	-0.001	26.304
	2:SELF	-10.294	488.854	0.141	0.332	-0.005	15.225
	3:LIVE	-4.150	121.208	-0.027	-0.013	0.003	6.093
	4:COMBINATK	-32.191	1.33E+3	0.409	1.193	-0.008	47.621
	5:COMBINATK	-40.290	1.85E+3	0.480	1.428	-0.012	59.582
	6:COMBINATK	-39.258	1.7E+3	0.610	1.689	-0.008	58.140
101	1:DEAD	-11.089	694.701	0.855	1.855	0.016	16.415
	2:SELF	-10.242	486.807	-0.005	0.070	0.011	15.134
	3:LIVE	-4.144	121.034	0.052	0.081	0.003	6.089
	4:COMBINATK	-25.478	1.28E+3	0.903	1.806	0.030	37.638
	5:COMBINATK	-32.229	1.59E+3	1.104	2.200	0.037	47.602
	6:COMBINATK	-29.864	1.63E+3	1.191	2.415	0.038	44.168
102	1:DEAD	-8.439	703.560	-0.330	-0.113	0.014	12.361
	2:SELF	-9.348	537.833	0.023	0.094	0.008	13.728
	3:LIVE	-3.202	127.080	-0.016	-0.031	0.002	4.688
	4:COMBINATK	-20.988	1.37E+3	-0.323	-0.049	0.024	30.755
	5:COMBINATK	-28.488	1.69E+3	-0.395	-0.071	0.030	38.773
	6:COMBINATK	-24.901	1.74E+3	-0.430	-0.025	0.031	36.522
103	1:DEAD	-16.549	752.326	0.150	0.594	0.021	24.449
	2:SELF	-10.074	468.107	0.088	0.164	0.013	14.845
	3:LIVE	-4.084	121.778	-0.088	-0.105	0.004	5.958
	4:COMBINATK	-30.887	1.34E+3	0.150	0.654	0.039	45.252
	5:COMBINATK	-38.450	1.86E+3	0.152	0.742	0.048	56.685
	6:COMBINATK	-37.273	1.71E+3	0.305	1.062	0.048	55.012
104	1:DEAD	-10.030	652.221	0.862	1.667	-0.001	14.710
	2:SELF	-9.607	464.398	-0.089	-0.070	0.005	14.100
	3:LIVE	-3.778	119.183	0.003	-0.003	0.000	5.523
	4:COMBINATK	-23.416	1.24E+3	0.776	1.593	0.004	34.334
	5:COMBINATK	-29.610	1.53E+3	0.933	1.910	0.005	43.410
	6:COMBINATK	-27.491	1.56E+3	1.062	2.235	0.005	40.334
105	1:DEAD	-13.474	549.540	-3.317	-4.514	-0.046	19.841
	2:SELF	-6.485	297.211	-2.188	-3.178	-0.013	9.443
	3:LIVE	-2.195	59.310	-0.851	-1.269	-0.005	3.178
	4:COMBINATK	-22.134	908.061	-8.358	-8.961	-0.085	32.481
	5:COMBINATK	-27.438	1.11E+3	-7.988	-11.261	-0.080	40.225
	6:COMBINATK	-27.915	1.19E+3	-7.708	-10.769	-0.084	40.996
106	1:DEAD	-0.488	364.886	0.151	0.690	-0.003	0.458
	2:SELF	-0.891	243.127	-0.097	-0.088	-0.004	1.117
	3:LIVE	-0.816	85.649	-0.212	-0.354	-0.001	1.105



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By yasir w j

Date 05-Dec-10

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**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	4 COMBINATK	-2.194	893.842	-0.159	0.247	-0.008	2.681
	5 COMBINATK	-2.860	886.830	-0.276	0.155	-0.010	3.660
	6 COMBINATK	-1.930	851.190	0.075	0.842	-0.009	2.206
107	1 DEAD	0.775	369.998	0.120	0.645	0.025	-1.265
	2 SELF	1.123	244.686	-0.040	0.067	0.016	-1.777
	3 LIVE	0.981	86.161	-0.171	-0.243	0.005	-1.498
	4 COMBINATK	2.859	700.825	-0.092	0.469	0.046	-4.540
	5 COMBINATK	3.815	875.454	-0.179	0.466	0.057	-6.047
	6 COMBINATK	2.658	860.530	0.111	0.997	0.057	-4.259
108	1 DEAD	-11.744	987.001	2.672	5.699	-0.172	0.107
	2 SELF	-6.331	944.713	2.513	4.136	-0.130	-4.424
	3 LIVE	-3.772	321.175	3.630	5.361	-0.091	-2.063
	4 COMBINATK	-21.847	2.25E+3	8.815	15.196	-0.393	-6.379
	5 COMBINATK	-27.725	2.83E+3	12.030	20.379	-0.508	-8.481
	6 COMBINATK	-25.304	2.7E+3	7.258	13.770	-0.423	-6.043
109	1 DEAD	2.007	89.749	-0.157	-0.347	0.013	0.080
	2 SELF	0.135	83.660	-0.815	-1.334	0.002	0.041
	3 LIVE	-2.775	27.895	-1.069	-1.645	-0.005	-0.182
	4 COMBINATK	-0.832	201.303	-2.041	-3.327	0.010	-0.071
	5 COMBINATK	-1.869	252.722	-2.877	-4.152	0.009	-0.161
	6 COMBINATK	3.000	242.772	-1.381	-2.354	0.021	0.170
110	1 DEAD	-4.756	83.041	-0.175	-0.409	-0.018	-0.784
	2 SELF	-2.757	80.246	-0.882	-1.447	-0.006	-0.703
	3 LIVE	0.623	26.477	-1.090	-1.675	-0.002	-0.205
	4 COMBINATK	-8.890	189.784	-2.147	-3.531	-0.028	-1.701
	5 COMBINATK	-8.019	238.307	-3.012	-4.908	-0.034	-2.124
	6 COMBINATK	-10.518	228.602	-1.480	-2.598	-0.036	-2.096
111	1 DEAD	21.834	973.524	2.416	5.291	0.313	-42.633
	2 SELF	13.555	938.944	2.054	3.043	0.314	-29.122
	3 LIVE	8.033	318.618	3.302	4.541	0.254	-16.485
	4 COMBINATK	43.422	2.23E+3	7.771	12.875	0.881	-88.239
	5 COMBINATK	55.320	2.8E+3	10.646	17.266	1.159	-112.481
	6 COMBINATK	49.544	2.68E+3	6.257	11.668	0.878	-100.456
112	1 DEAD	3.937	492.694	1.935	3.341	0.010	-6.007
	2 SELF	3.865	416.840	1.545	2.395	0.001	-5.899
	3 LIVE	2.617	202.568	1.607	2.408	-0.003	-3.989
	4 COMBINATK	10.419	1.11E+3	5.087	8.143	0.007	-15.895
	5 COMBINATK	13.549	1.42E+3	6.747	10.734	0.008	-20.869
	6 COMBINATK	10.923	1.27E+3	4.872	8.031	0.015	-16.868
113	1 DEAD	-8.925	309.015	-1.636	-1.972	0.033	10.180
	2 SELF	-4.543	260.536	-0.853	-1.147	0.019	6.616
	3 LIVE	-0.831	41.969	-0.051	-0.046	0.002	1.139
	4 COMBINATK	-12.289	611.520	-2.541	-3.165	0.055	17.935
	5 COMBINATK	-15.081	750.812	-3.070	-3.817	0.067	21.977



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By yasir w.j	Date 05-Dec-10	Chd Dr alaa k
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**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
114	6-COMBINATK	-18.055	797.371	-3.486	-4.367	0.073	23.514
	1-DEAD	0.759	72.291	18.439	-6.484	-1.330	1.279
	2-SELF	0.283	83.841	22.989	-7.514	-1.816	1.706
	3-LIVE	-0.931	42.961	9.977	-4.435	-0.952	1.084
	4-COMBINATK	0.111	199.193	51.405	-18.433	-3.899	4.070
	5-COMBINATK	-0.240	256.218	65.677	-23.893	-5.059	5.317
115	6-COMBINATK	1.459	218.724	58.000	-19.596	-4.125	4.180
	1-DEAD	0.241	83.708	-19.315	6.288	-0.035	-0.154
	2-SELF	0.989	114.124	-25.293	8.623	-0.126	-0.499
	3-LIVE	0.814	74.351	-16.714	5.606	-0.090	-0.326
	4-COMBINATK	2.044	272.182	-61.322	20.497	-0.251	-0.980
	5-COMBINATK	2.778	356.359	-80.272	26.838	-0.337	-1.306
116	6-COMBINATK	1.722	276.964	-62.451	20.847	-0.226	-0.915
	1-DEAD	12.935	86.881	-0.275	-0.016	0.013	7.094
	2-SELF	11.528	77.619	-0.181	-0.015	0.008	6.297
	3-LIVE	2.416	14.621	-0.049	-0.011	0.004	1.149
	4-COMBINATK	26.878	179.121	-0.505	-0.042	0.024	14.539
	5-COMBINATK	33.218	220.793	-0.825	-0.055	0.030	17.907
117	6-COMBINATK	34.245	230.299	-0.839	-0.044	0.028	18.747
	1-DEAD	8.623	201.447	1.583	2.251	-0.472	-1.556
	2-SELF	-10.665	215.058	0.873	0.960	0.346	-1.113
	3-LIVE	-0.141	29.244	0.849	0.779	-0.164	-0.711
	4-COMBINATK	-19.428	445.749	3.105	3.990	-0.983	-3.379
	5-COMBINATK	-23.371	548.596	3.985	5.099	1.245	-4.340
118	6-COMBINATK	-27.002	583.107	3.439	4.495	-1.146	-3.736
	1-DEAD	8.277	169.031	14.950	-7.295	-0.073	6.501
	2-SELF	8.127	151.187	12.885	-6.682	-0.044	5.685
	3-LIVE	1.665	27.128	2.666	-1.191	-0.005	0.931
	4-COMBINATK	18.070	347.346	30.502	-15.169	-0.122	13.117
	5-COMBINATK	22.350	427.966	37.669	-18.879	-0.148	16.113
119	6-COMBINATK	22.966	446.305	38.970	-19.568	-0.164	17.060
	1-DEAD	14.104	123.781	-12.953	6.895	-0.181	0.482
	2-SELF	13.587	126.286	-13.652	6.873	-0.157	0.608
	3-LIVE	3.337	24.447	-1.972	1.338	-0.049	0.028
	4-COMBINATK	31.028	274.493	-28.578	15.106	-0.337	1.118
	5-COMBINATK	38.568	339.171	-35.063	18.663	-0.484	1.353
120	6-COMBINATK	38.767	350.066	-37.248	19.275	-0.473	1.527
	1-DEAD	13.966	551.301	-3.169	-4.146	0.067	-21.132
	2-SELF	6.820	296.301	-2.143	-3.070	0.032	-10.429
	3-LIVE	2.391	58.732	-0.640	-1.257	0.017	-3.729
	4-COMBINATK	23.177	909.335	-6.160	-8.473	0.117	-35.289
	5-COMBINATK	28.769	1.12E+3	-7.731	-10.871	0.147	-43.839
121	6-COMBINATK	29.101	1.19E+3	-7.436	-10.102	0.139	-44.185
	1-DEAD	-18.509	185.517	17.031	-7.699	-0.021	-6.470



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Job No

Sheet No

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Job Title building department

Part

Ref

By yasir w j

Date 05-Dec-10

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**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	2 SELF	-14.636	164.121	15.112	-8.919	-0.023	-5.678
	3 LIVE	-1.751	24.751	2.816	-1.017	0.009	-0.917
	4 COMBINATK	-32.896	374.389	34.959	-15.636	-0.035	-13.064
	5 COMBINATK	-40.176	459.187	43.078	-19.170	-0.038	-16.044
	6 COMBINATK	-43.804	489.493	45.000	-20.486	-0.061	-17.006
122	1 DEAD	5.583	41.555	0.137	0.043	-0.012	2.101
	2 SELF	6.535	44.317	0.091	-0.003	-0.001	2.171
	3 LIVE	1.045	7.951	0.043	0.014	-0.004	0.397
	4 COMBINATK	13.162	93.823	0.271	0.054	-0.017	4.668
	5 COMBINATK	16.212	115.768	0.342	0.071	-0.021	5.761
	6 COMBINATK	18.964	120.221	0.319	0.056	-0.017	5.981
123	1 DEAD	-16.718	133.971	-11.372	7.523	0.226	-0.486
	2 SELF	-15.922	132.759	-11.543	7.320	0.202	-0.564
	3 LIVE	-2.959	21.116	-1.349	1.180	0.042	-0.068
	4 COMBINATK	-35.597	287.846	-24.284	16.023	0.470	-1.098
	5 COMBINATK	-43.900	353.861	-29.657	19.699	0.581	-1.344
	6 COMBINATK	-45.893	373.422	-32.081	20.780	0.600	-1.442
124	1 DEAD	7.901	809.645	-2.356	-3.035	-0.012	-11.873
	2 SELF	4.845	431.427	-1.527	-2.166	-0.015	-7.365
	3 LIVE	0.409	47.993	0.143	0.232	-0.005	-0.725
	4 COMBINATK	13.156	1.09E+3	-3.741	-4.969	-0.031	-19.963
	5 COMBINATK	15.951	1.33E+3	-4.432	-5.869	-0.040	-24.245
	6 COMBINATK	17.845	1.48E+3	-5.437	-7.281	-0.037	-26.933
125	1 DEAD	-7.951	817.252	-2.353	-3.039	0.020	11.733
	2 SELF	-4.769	435.208	-1.477	-2.073	0.010	6.970
	3 LIVE	-0.256	49.142	0.185	0.272	0.001	0.292
	4 COMBINATK	-12.976	1.1E+3	-3.665	-4.841	0.031	18.994
	5 COMBINATK	-15.674	1.34E+3	-4.333	-5.700	0.037	22.910
	6 COMBINATK	-17.808	1.47E+3	-5.362	-7.157	0.042	26.183
129	1 DEAD	-5.739	44.668	1.266	0.229	0.063	-1.882
	2 SELF	-7.752	44.539	0.766	-0.327	-0.104	-1.583
	3 LIVE	-5.475	19.495	0.344	-0.574	-0.176	-0.421
	4 COMBINATK	-18.985	108.702	2.376	-0.872	-0.217	-3.886
	5 COMBINATK	-24.948	136.241	2.989	-1.036	-0.331	-4.831
	6 COMBINATK	-18.867	124.890	2.846	-0.137	-0.057	-4.851
130	1 DEAD	-13.193	107.848	-3.389	-2.108	0.209	3.181
	2 SELF	-10.581	99.134	-3.124	-2.776	0.132	2.870
	3 LIVE	-3.312	27.721	-2.539	-2.818	0.080	1.162
	4 COMBINATK	-27.086	234.501	-9.051	-7.502	0.422	7.213
	5 COMBINATK	-33.827	292.489	-11.877	-10.050	0.538	9.121
	6 COMBINATK	-33.283	289.482	-9.117	-8.836	0.478	8.471
131	1 DEAD	12.890	111.117	-3.302	-1.989	-0.160	-3.059
	2 SELF	9.983	99.716	-3.069	-2.606	-0.094	-2.691
	3 LIVE	2.505	28.614	-2.550	-2.527	-0.047	-1.511

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Job Title building department	Ref		
Client university of technology	By yasir w.j	Date 05-Dec-10	Chd Dr alaa k
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## Reactions Cont...

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	4-COMBINATK	25.378	239.447	-8.940	-7.122	-0.302	-7.261
	5-COMBINATK	31.455	298.782	-11.748	-8.557	-0.381	-8.317
	6-COMBINATK	32.022	295.166	-8.947	-6.433	-0.356	-8.050
132	1-DEAD	-23.089	80.350	-2.487	-1.314	-0.388	-3.352
	2-SELF	-19.394	71.096	-2.028	-1.861	-0.461	-3.055
	3-LIVE	-4.522	17.467	-1.527	1.545	-0.421	-0.686
	4-COMBINATK	-48.985	168.913	-8.042	-4.520	-1.271	-7.093
	5-COMBINATK	-58.191	209.682	-7.861	-8.042	-1.693	8.786
	6-COMBINATK	-59.448	212.024	-8.321	-4.166	-1.189	-8.969
133	1-DEAD	20.861	74.175	-2.271	-1.148	0.343	2.358
	2-SELF	16.967	64.099	-1.913	-1.453	0.417	2.134
	3-LIVE	2.981	14.338	-1.468	-1.393	0.394	0.355
	4-COMBINATK	40.788	152.813	-5.651	-3.991	1.153	4.846
	5-COMBINATK	50.130	188.871	-7.369	-5.347	1.541	5.957
	6-COMBINATK	52.958	193.585	-5.857	-3.638	1.063	6.288
140	1-DEAD	-5.493	5.768	9.169	-0.690	0.264	-0.312
	2-SELF	-5.291	9.600	10.386	-2.369	0.300	1.065
	3-LIVE	-3.649	7.853	7.570	-2.354	0.160	-0.983
	4-COMBINATK	-14.434	23.220	27.126	-5.414	0.724	-2.360
	5-COMBINATK	-18.780	31.005	35.579	-7.439	0.933	-3.225
	6-COMBINATK	-15.098	21.515	27.377	-4.283	0.789	-1.928
143	1-DEAD	1.423	11.684	13.968	-1.762	-0.924	1.375
	2-SELF	2.756	14.835	15.922	-3.051	-0.749	1.750
	3-LIVE	2.364	11.708	11.544	-2.870	-0.419	1.457
	4-COMBINATK	6.543	38.228	41.434	-7.682	-2.092	4.582
	5-COMBINATK	8.797	50.554	54.338	-10.367	-2.678	6.081
	6-COMBINATK	5.851	37.126	41.846	-8.738	-2.342	4.375
150	1-DEAD	-2.118	850.087	-8.619	-13.596	0.155	-0.103
	2-SELF	-0.781	733.985	-7.659	-11.680	0.215	-1.250
	3-LIVE	-0.445	326.814	-7.180	-11.091	0.174	-0.655
	4-COMBINATK	-3.324	1.91E+3	-24.457	-36.347	0.544	-2.008
	5-COMBINATK	-4.167	2.42E+3	-32.221	-48.052	0.722	-2.672
	6-COMBINATK	-4.032	2.22E+3	-24.189	-35.358	0.518	-1.894
164	1-DEAD	52.493	370.109	-29.950	22.716	-0.630	7.266
	2-SELF	27.580	281.554	-22.279	14.790	-0.367	6.071
	3-LIVE	6.675	75.248	-6.048	3.933	-0.206	1.852
	4-COMBINATK	88.727	706.911	-58.277	41.440	-1.203	15.189
	5-COMBINATK	108.742	878.392	-72.351	51.301	-1.528	18.967
	6-COMBINATK	112.074	884.328	-73.121	52.509	-1.396	18.671
165	1-DEAD	-52.840	352.158	-32.093	21.582	0.671	-8.312
	2-SELF	-24.072	242.575	-24.807	14.192	0.379	-5.120
	3-LIVE	-3.418	81.073	-7.966	3.378	0.216	-1.130
	4-COMBINATK	-80.431	655.805	-64.866	39.150	1.268	-12.562
	5-COMBINATK	-97.684	811.395	-81.025	48.331	1.606	-15.527



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Job No	Sheet No <b>18</b>	Rev
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Job Title building department

Client university of technology

**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	6.COMBINATK	-107.818	832.626	-79.660	50.084	1.470	-16.006
166	1.DEAD	0.895	148.505	15.824	-24.389	1.033	-2.997
	2.SELF	0.533	82.685	5.393	-15.785	0.378	-1.840
	3.LIVE	1.618	-9.788	-9.530	-4.201	0.180	-0.656
	4.COMBINATK	3.046	222.602	11.788	-44.375	1.591	-5.492
	5.COMBINATK	4.303	263.208	10.334	-54.931	1.982	-6.852
	6.COMBINATK	1.999	325.347	29.845	-56.244	1.975	-6.771
167	1.DEAD	0.517	148.593	13.202	-24.411	-0.380	1.643
	2.SELF	1.337	88.844	7.768	-15.182	0.184	0.341
	3.LIVE	-0.275	-5.384	-7.608	-3.718	0.198	-0.416
	4.COMBINATK	1.579	230.044	13.362	-43.312	0.001	1.568
	5.COMBINATK	1.785	273.895	12.992	-53.461	0.081	1.715
	6.COMBINATK	2.596	329.812	29.358	-55.431	-0.275	2.778
168	1.DEAD	48.830	131.496	-10.782	-2.767	0.897	10.955
	2.SELF	23.948	90.843	-7.162	-2.560	0.828	7.701
	3.LIVE	1.828	13.808	-2.722	-1.958	0.583	2.309
	4.COMBINATK	74.606	235.947	-20.666	-7.285	2.409	20.966
	5.COMBINATK	90.258	288.579	-25.887	-9.525	3.124	26.082
	6.COMBINATK	101.889	311.275	-25.122	-7.457	2.556	26.119
169	1.DEAD	-40.819	106.248	-10.778	-3.460	-1.277	-10.808
	2.SELF	-18.187	68.033	-6.848	-2.655	-1.178	-7.842
	3.LIVE	1.512	-1.297	-2.622	-2.020	-0.773	-2.455
	4.COMBINATK	-57.294	172.982	-20.245	-8.135	-3.228	-21.105
	5.COMBINATK	-68.148	207.060	-25.343	-10.569	-4.183	-26.308
	6.COMBINATK	-82.328	243.990	-24.873	-8.560	3.437	-26.110
176	1.DEAD	4.764	876.771	-10.450	-14.735	-0.047	-9.131
	2.SELF	2.316	740.590	-7.611	-11.152	0.061	-5.129
	3.LIVE	1.317	324.083	-6.987	-10.440	0.048	-2.799
	4.COMBINATK	8.396	1.94E+3	-25.049	-36.327	0.062	-17.059
	5.COMBINATK	10.602	2.46E+3	-32.854	-47.768	0.093	-21.590
	6.COMBINATK	9.911	2.26E+3	-25.286	-36.242	0.019	-19.964
243	1.DEAD	6.366	75.198	-2.204	-0.514	-0.095	0.433
	2.SELF	5.497	78.073	-2.225	-0.586	-0.103	0.460
	3.LIVE	1.886	14.548	-0.364	-0.083	-0.010	0.058
	4.COMBINATK	13.749	187.819	-4.794	-1.183	-0.208	0.951
	5.COMBINATK	17.253	207.203	-5.699	-1.453	-0.254	1.165
	6.COMBINATK	16.608	214.579	-6.202	-1.539	-0.276	1.250
244	1.DEAD	-8.234	83.311	-1.896	-0.447	0.062	-0.579
	2.SELF	-7.435	84.073	-1.864	-0.490	0.063	-0.589
	3.LIVE	-1.831	13.780	-0.260	-0.059	0.008	-0.116
	4.COMBINATK	-17.300	181.184	-4.023	-0.996	0.173	-1.285
	5.COMBINATK	-21.412	222.909	-4.931	-1.219	0.211	-1.588
	6.COMBINATK	-21.936	234.337	-5.287	-1.312	0.232	-1.636
245	1.DEAD	-3.486	82.531	-0.177	-0.047	0.002	-0.061



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**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	2 SELF	-2.529	84.734	-0.192	-0.115	0.003	-0.062
	3 LIVE	-0.751	14.854	-0.035	-0.004	0.000	-0.042
	4 COMBINATK	-6.766	182.119	-0.404	-0.166	0.005	-0.165
	5 COMBINATK	-8.419	224.485	-0.499	-0.200	0.006	-0.215
	6 COMBINATK	-8.421	234.171	-0.517	-0.227	0.007	-0.172
248	1 DEAD	3.682	72.583	-0.183	0.019	0.009	-0.061
	2 SELF	2.525	75.989	-0.184	-0.080	0.005	-0.058
	3 LIVE	1.510	12.532	-0.042	0.019	0.004	-0.036
	4 COMBINATK	7.717	161.104	-0.409	-0.042	0.017	-0.155
	5 COMBINATK	9.864	196.337	-0.508	-0.043	0.022	-0.200
	6 COMBINATK	8.689	208.000	-0.514	-0.086	0.019	-0.167
447	1 DEAD	-7.487	788.780	5.794	9.089	0.016	10.908
	2 SELF	-3.153	458.787	3.611	5.456	-0.007	4.458
	3 LIVE	-1.350	89.010	1.394	2.075	-0.005	1.865
	4 COMBINATK	-11.990	1.34E+3	10.799	16.620	0.005	17.231
	5 COMBINATK	-14.928	1.64E+3	13.516	20.774	0.003	21.424
	6 COMBINATK	-14.896	1.75E+3	13.187	20.363	0.014	21.512
740	1 DEAD	6.830	286.009	2.116	-2.676	-0.021	-10.264
	2 SELF	4.522	239.755	-1.347	-1.897	-0.023	-6.860
	3 LIVE	0.928	35.199	-0.208	-0.286	-0.007	-1.484
	4 COMBINATK	12.280	560.964	-3.671	-4.858	-0.050	-18.608
	5 COMBINATK	15.107	687.236	-4.489	-5.944	-0.063	-22.923
	6 COMBINATK	15.892	736.070	-4.848	-6.401	-0.061	-23.974
1295	1 DEAD	-2.975	7.144	5.513	-1.062	0.259	-0.653
	2 SELF	-4.367	11.295	5.914	-2.534	0.065	-1.120
	3 LIVE	-4.276	12.594	8.049	-2.244	0.280	-1.195
	4 COMBINATK	-11.617	31.033	19.475	-5.839	0.604	-2.989
	5 COMBINATK	-15.651	42.277	26.590	-7.904	0.836	-4.041
	6 COMBINATK	-10.278	25.815	15.997	-5.034	0.454	-2.483
8558	1 DEAD	1.315	70.152	0.092	0.168	0.001	-0.041
	2 SELF	0.310	73.918	0.012	0.034	0.003	-0.023
	3 LIVE	0.986	11.233	0.047	0.063	-0.001	-0.040
	4 COMBINATK	2.611	155.303	0.151	0.265	0.003	-0.104
	5 COMBINATK	3.528	190.857	0.200	0.343	0.003	-0.141
	6 COMBINATK	2.275	201.696	0.145	0.282	0.006	0.090
8585	1 DEAD	5.728	75.855	-0.881	-0.178	-0.023	-0.113
	2 SELF	4.584	78.916	-0.646	-0.257	-0.026	-0.112
	3 LIVE	1.896	13.889	-0.137	-0.026	-0.002	-0.045
	4 COMBINATK	12.208	168.440	-1.445	-0.481	-0.053	-0.270
	5 COMBINATK	15.408	207.676	-1.788	-0.563	-0.064	-0.343
	6 COMBINATK	14.437	216.400	-1.830	-0.500	-0.071	-0.315
8897	1 DEAD	0.996	157.281	3.616	0.697	-0.103	-0.489
	2 SELF	0.931	148.757	2.451	0.229	-0.106	-0.464
	3 LIVE	0.247	26.439	1.118	0.044	-0.021	-0.161





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Job Title buiding department

Client university of tecnology

**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	4.COMBINATK	2.175	330.477	7.188	0.970	-0.230	-1.114
	5.COMBINATK	2.709	407.148	9.070	1.182	-0.284	-1.401
	6.COMBINATK	2.700	425.653	8.495	1.296	-0.293	-1.334
6698	1.DEAD	2.323	150.616	-3.120	0.155	0.302	-0.939
	2.SELF	2.151	148.214	-3.947	-0.292	0.290	-0.857
	3.LIVE	0.558	27.430	0.382	-0.099	0.071	-0.267
	4.COMBINATK	5.030	328.258	-6.705	-0.237	0.662	-2.063
	5.COMBINATK	6.259	402.453	-7.901	-0.323	0.823	-2.583
	6.COMBINATK	6.263	418.382	-9.894	-0.193	0.828	-2.515
6787	1.DEAD	-7.006	85.316	-0.803	-0.188	0.030	-0.016
	2.SELF	-6.001	86.827	-0.591	-0.241	0.031	-0.013
	3.LIVE	-1.417	14.727	-0.105	-0.028	0.004	-0.031
	4.COMBINATK	-14.424	186.889	-1.299	-0.456	0.064	-0.061
	5.COMBINATK	-17.875	230.133	-1.601	-0.559	0.079	-0.085
	6.COMBINATK	-18.210	240.999	-1.671	-0.600	0.085	-0.041
6801	1.DEAD	1.329	78.917	0.084	0.049	0.007	0.024
	2.SELF	2.077	82.225	0.018	-0.037	0.008	-0.002
	3.LIVE	0.180	14.787	0.032	0.019	0.002	-0.028
	4.COMBINATK	3.587	175.939	0.134	0.030	0.017	-0.007
	5.COMBINATK	4.377	217.045	0.174	0.044	0.022	-0.019
	6.COMBINATK	4.789	225.589	0.142	0.016	0.022	0.030
7073	1.DEAD	-2.061	187.240	5.768	0.829	0.282	0.939
	2.SELF	-1.791	153.488	5.235	0.378	0.248	0.812
	3.LIVE	-0.238	23.282	1.722	0.043	0.029	0.098
	4.COMBINATK	-4.088	344.008	12.728	1.251	0.560	1.848
	5.COMBINATK	-5.000	422.123	15.980	1.518	0.683	2.256
	6.COMBINATK	-5.383	448.017	15.405	1.890	0.742	2.452
7074	1.DEAD	-2.507	160.733	0.817	0.014	-0.360	1.121
	2.SELF	-2.325	154.585	0.422	-0.365	-0.342	1.005
	3.LIVE	-0.439	24.018	0.953	-0.087	-0.065	0.171
	4.COMBINATK	-5.271	339.334	2.192	-0.418	-0.768	2.297
	5.COMBINATK	-6.501	418.808	3.011	-0.528	-0.947	2.824
	6.COMBINATK	-6.765	441.448	1.734	-0.492	-0.984	2.976
7081	1.DEAD	3.818	158.583	-0.061	0.128	-0.040	-0.038
	2.SELF	3.028	141.351	-0.025	0.089	-0.030	-0.107
	3.LIVE	1.068	24.587	-0.032	0.003	-0.005	-0.125
	4.COMBINATK	7.711	324.532	-0.118	0.220	-0.076	-0.270
	5.COMBINATK	9.680	399.277	-0.154	0.266	-0.093	-0.374
	6.COMBINATK	9.303	419.809	-0.121	0.304	-0.098	-0.203
7085	1.DEAD	-4.187	180.886	1.998	0.706	-0.271	0.336
	2.SELF	-3.889	142.403	1.727	0.572	-0.237	0.235
	3.LIVE	0.100	22.754	0.305	0.101	-0.046	-0.049
	4.COMBINATK	-7.956	328.143	4.030	1.379	-0.554	0.522
	5.COMBINATK	-9.507	400.474	4.958	1.695	-0.683	0.607



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Job No	Sheet No <b>21</b>	Rev
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Job Title building department

Client university of tecnologia

**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	6 COMBINATK	-11 278	424.745	5.215	1 789	-0 711	0 799
7108	1 DEAD	16 048	187 524	-0.806	-0 182	0 061	-5 183
	2 SELF	14 551	183.828	-0.562	-0 169	0 040	-4 546
	3 LIVE	2 066	22.944	-0 154	-0.052	0 010	-0 726
	4 COMBINATK	32.665	374.293	-1 522	-0 402	0 111	-10 456
	5 COMBINATK	40.024	458 329	-1.888	-0 504	0 137	-12 837
	6 COMBINATK	42.838	491 889	-1 915	-0 491	0 141	-13 821
7107	1 DEAD	-3 988	184.216	1 506	0 424	0 284	-0 003
	2 SELF	-2 347	144 895	1.272	0 309	0 237	-0 041
	3 LIVE	-0 187	23 010	0 250	0 059	0 050	-0 140
	4 COMBINATK	-8 503	332.121	3 028	0 792	0 571	-0 184
	5 COMBINATK	-7 879	407 749	3 734	0 974	0 705	-0 277
	6 COMBINATK	-8.842	432 755	3 890	1 026	0 729	-0 062
7315	1 DEAD	0 249	132.863	-17 808	-1 270	0 028	-0 263
	2 SELF	1 302	180 187	-20.160	-1 714	0 080	-0 929
	3 LIVE	0 985	113 674	-13 349	-1 170	0 062	-0 586
	4 COMBINATK	2.537	426.523	-51.318	-4 154	0 170	-1 778
	5 COMBINATK	3 438	557.297	-66.921	-5 452	0 229	-2 367
	6 COMBINATK	2 172	437.989	-53 158	-4 177	0 151	-1 668
7320	1 DEAD	0 108	124 442	-16.028	-0 769	0 020	-0 185
	2 SELF	1.320	183 211	-16 973	-1.162	0 056	-0 638
	3 LIVE	0.995	99 679	-11.780	-0.837	0 045	-0 340
	4 COMBINATK	2.423	387 331	-44.782	-2 768	0 121	-1 143
	5 COMBINATK	3 305	504 669	-58 450	-3.657	0 163	-1 507
	6 COMBINATK	1.999	402 714	-48 202	-2 703	0 106	-1 124
7321	1 DEAD	-0.097	119 442	-14.542	-1 503	-0.016	-0 091
	2 SELF	0 829	150 094	-14 773	-1 923	0 118	-0 400
	3 LIVE	0.619	88 300	-10 600	-1.290	0 087	-0 131
	4 COMBINATK	1 351	357 835	-39 915	-4 716	0 189	-0 622
	5 COMBINATK	1 868	464 723	-52.137	-6 175	0 262	-0 798
	6 COMBINATK	1 025	377 349	-41 041	-4 796	0 143	-0 687
7322	1 DEAD	-0.448	120.034	-2.621	-0.743	-0 037	-0 111
	2 SELF	0 621	142 745	-0.913	-1 086	0 087	-0 039
	3 LIVE	0 235	80.319	-1.869	-0.804	0 064	0 180
	4 COMBINATK	0.410	343 098	-5 403	-2.634	0 113	0 030
	5 COMBINATK	0.586	443 848	-7 231	3.482	0 162	0 108
	6 COMBINATK	0.245	367 891	-4.948	-2.561	0 069	-0 210
7422	1 DEAD	-4 328	21 654	20.855	-1 578	0 179	-0 631
	2 SELF	-6 286	27 879	25 940	-2 594	0 241	-0 785
	3 LIVE	-4 734	17 889	18.291	-1 936	-0.096	-0 257
	4 COMBINATK	-15 346	67.423	63.066	-6 107	0 324	-1 673
	5 COMBINATK	-20.308	88 063	82.220	-8 103	0 350	-2 111
	6 COMBINATK	-14 855	89.347	65 514	-5.840	0 587	-1 982
7423	1 DEAD	-3 745	14.236	13.267	-1 709	0.236	-0 095



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Job No

Sheet No

22

Rev

Part

Ref

By yasir w.j

Date 05-Dec-10

Chd Dr alaa k.

Job Title building department

Client university of technology

File design2.std

Date/Time 10-May-2011 09:36

**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	2:SELF	-5.552	20.371	15.389	-3.881	0.389	-0.085
	3:LIVE	-4.355	18.528	14.071	-3.345	0.001	0.223
	4:COMBINATK	-13.652	53.133	42.727	-8.915	0.627	0.043
	5:COMBINATK	-18.125	71.171	56.901	-12.036	0.752	0.141
	6:COMBINATK	-13.018	48.450	40.118	-7.798	0.875	-0.252
7595	1:DEAD	-5.050	11.737	18.383	-1.809	1.427	-0.564
	2:SELF	-4.303	18.602	19.214	-4.921	1.412	-0.629
	3:LIVE	-2.881	15.309	14.187	-4.836	0.934	-0.400
	4:COMBINATK	-12.234	45.847	49.784	-11.566	3.772	-1.593
	5:COMBINATK	-15.833	60.901	65.383	-15.813	4.900	-2.072
	6:COMBINATK	-13.094	42.474	49.836	-8.422	3.974	-1.671
7599	1:DEAD	-1.023	19.878	24.499	-3.034	2.120	-1.091
	2:SELF	-0.543	25.690	27.483	-5.692	2.006	-1.113
	3:LIVE	-0.151	20.248	19.740	-5.428	1.352	-0.743
	4:COMBINATK	1.717	65.816	71.701	-14.154	5.478	-2.947
	5:COMBINATK	-2.121	87.078	93.938	-19.155	7.115	-3.834
	6:COMBINATK	-2.182	63.795	72.746	-12.217	5.778	-3.086
7724	1:DEAD	-10.565	84.360	-1.084	-1.035	-0.035	0.166
	2:SELF	-7.823	79.881	-1.524	-1.875	-0.024	0.167
	3:LIVE	-1.743	24.504	-1.524	-1.949	-0.015	0.256
	4:COMBINATK	-20.131	188.745	-4.112	-4.858	-0.074	0.589
	5:COMBINATK	-24.854	238.298	-5.544	-8.810	-0.094	0.809
	6:COMBINATK	-25.743	229.938	-3.823	-4.074	-0.082	0.466
7737	1:DEAD	8.735	95.256	-1.096	-1.035	0.027	-0.901
	2:SELF	5.869	87.398	-1.528	-1.883	0.021	-0.821
	3:LIVE	0.008	27.293	-1.564	-2.014	0.015	-0.761
	4:COMBINATK	14.612	209.848	-4.188	-4.911	0.063	-2.483
	5:COMBINATK	17.538	262.855	-5.651	-8.699	0.082	-3.284
	6:COMBINATK	20.448	255.717	-3.874	-4.056	0.067	-2.410
7748	1:DEAD	-10.245	83.590	1.657	0.386	-0.113	1.197
	2:SELF	-10.145	79.759	0.740	-0.686	-0.119	1.111
	3:LIVE	-6.143	29.268	0.048	-1.165	-0.102	0.433
	4:COMBINATK	-28.533	192.616	2.446	-1.466	-0.333	2.741
	5:COMBINATK	-34.297	242.847	2.954	-2.225	-0.441	3.483
	6:COMBINATK	-28.548	228.888	3.356	-0.421	-0.324	3.232
7755	1:DEAD	2.233	40.120	1.282	0.192	-0.052	2.086
	2:SELF	4.959	42.252	0.891	-0.418	0.130	1.840
	3:LIVE	3.266	17.290	0.276	-0.830	0.193	0.588
	4:COMBINATK	10.458	99.661	2.229	-0.856	0.271	4.514
	5:COMBINATK	13.855	126.509	2.785	-1.279	0.402	5.652
	6:COMBINATK	10.068	115.320	2.734	-0.318	0.110	5.496
7758	1:DEAD	6.553	79.778	1.832	0.313	0.117	-1.125
	2:SELF	6.904	79.366	0.590	-0.885	0.121	-1.080
	3:LIVE	3.897	28.823	-0.069	1.273	0.100	-0.453



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Job No	Sheet No <b>23</b>	Rev
Part		
Ref		
By yasir w.j	Date 05-Dec-10	Chd Dr alaa k
Client university of technology	File design2.std	Date/Time 10-May-2011 09:36

**Reactions Cont...**

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
	4-COMBINATIC	17.154	187.785	2.154	-1.828	0.337	-2.658
	5-COMBINATIC	22.084	236.787	2.557	-2.700	0.444	-3.370
	6-COMBINATIC	18.840	222.799	3.111	-0.774	0.332	-3.086
7822	1-DEAD	-9.086	707.031	-0.212	0.102	0.006	13.490
	2-SELF	-10.116	529.869	0.068	0.202	0.002	14.964
	3-LIVE	-3.598	122.673	0.006	0.028	-0.001	5.282
	4-COMBINATK	-22.800	1.38E+3	-0.138	0.331	0.008	33.736
	5-COMBINATK	-28.799	1.68E+3	-0.163	0.407	0.009	42.596
	6-COMBINATK	-26.882	1.73E+3	-0.202	0.427	0.012	39.636
9200	1-DEAD	-3.828	509.043	1.314	2.410	0.005	5.805
	2-SELF	-3.991	433.326	1.017	1.630	0.000	5.818
	3-LIVE	-2.591	206.929	1.456	2.186	0.001	3.754
	4-COMBINATK	-10.410	1.15E+3	3.786	6.226	0.006	15.177
	5-COMBINATK	-13.528	1.48E+3	5.126	8.346	0.008	19.714
	6-COMBINATK	-10.946	1.32E+3	3.263	5.656	0.007	15.992
9201	1-DEAD	-0.860	416.865	0.800	1.661	-0.004	0.993
	2-SELF	-0.864	272.562	0.362	0.613	-0.006	1.060
	3-LIVE	-0.788	101.749	0.195	0.271	-0.004	1.053
	4-COMBINATK	-2.512	791.177	1.358	2.545	-0.014	3.106
	5-COMBINATK	-3.329	990.112	1.707	3.162	-0.019	4.148
	6-COMBINATK	-2.414	965.198	1.628	3.184	-0.014	2.673
9202	1-DEAD	1.063	424.129	0.906	1.817	0.025	-1.614
	2-SELF	1.052	275.413	0.523	0.907	0.015	-1.621
	3-LIVE	0.829	102.534	0.297	0.457	0.004	-1.435
	4-COMBINATK	3.044	802.075	1.726	3.182	0.045	-4.671
	5-COMBINATK	4.025	1E+3	2.190	4.001	0.056	-6.179
	6-COMBINATK	2.961	979.358	2.000	3.614	0.057	-4.530



STAAD SPACE

PAGE NO 103

225J 2100X 300X 600 42

5No12 @ 543. 60 TO 2100

3\*120/C2

5No12 @ 57. 0 TO 1378

1	00000	00000	00000	00000
5#12	5#12	5#12	5#12	5#12
5#12	5#12	5#12	5#12	5#12
00000	00000	00000	00000	00000

## BEAM NO. 120 DESIGN RESULTS FLEXURE PER CODE ACT 918-05

LEN 4200 MM FY - 414. FC - 28. MPA, SIZE - 300 X 600 MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57	5 12MM	543	3828	NO NO
2	543	5 12MM	0	1144	YES NO
3	543.	5 12MM	2881	4200.	NO YES

## BEAM NO. 120 DESIGN RESULTS - SHEAR

AT START SUPPORT -  $V_u = 70.43$  KNS  $V_c = 150.68$  KNS  $V_s = 0.00$  KNS  
 $T_u = 0.14$  KN-MET  $T_c = 6.1$  KN MET  $T_s = 0.0$  KN-MET LOAD 2  
 NO STIRRUPS ARE REQUIRED FOR TORSION.

REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1

PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272 MM C/C FOR 1563. MM

AT END SUPPORT -  $V_u = 42.08$  KNS  $V_c = 193.16$  KNS  $V_s = 0.00$  KNS  
 $T_u = 0.10$  KN MET  $T_c = 6.0$  KN MET  $T_s = 0.0$  KN-MET LOAD  
 STIRRUPS ARE NOT REQUIRED.

STAAD SPACE

- PAGE NO. 104

42T 4199X 300X 600 43T

5No12 H 543. 0. TO 1144 5No12 H 543 288. TO 4200

7\*12/c272

5No12 H 57 547 TO 3828

00000	00000			00000	00000
5#12	5#12			5#12	5#12
	5#12	5#12	5#12	5#12	
	00000	00000	00000	00000	

# BEAM NO. 121 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200. MM FY - 414. FC - 28. MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	57.	5 - 12MM	547	3478.	NO	NO
2	543.	5 - 12MM	0.	1144	YES	NO
3	543	5 - 12MM	288.1.	4200	NO	YES

# BEAM NO 121 DESIGN RESULTS - SHEAR

AT START SUPPORT Vu= 65.66 KNS Vc= 153.69 KNS Vs= 0.00 KNS  
 Tu= 0.19 KN MET Tc= 6.0 KN MET Ts= 0.0 KN MET LOAD  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT FOR SHEAR IS PER CL 11.5 5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272. MM C/C FOR 1564. MM

AT END SUPPORT Vu= 65.68 KNS Vc= 153.84 KNS Vs= 0.00 KNS  
 Tu= 0.19 KN MET Tc= 6.0 KN MET Ts= 0.0 KN-MET LOAD  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT FOR SHEAR IS PER CL 11.5 5.1.  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272 MM C/C FOR 1564. MM

STAAD SPACE

PAGE NO 105

44 4200X 300X 600 445

5No12 H 543. 0. TO 1144 5No12 H 543. 231. TO 4200  
7\*12c/c272 7\*12c/c272  
5No12 H 57 547. TO 3478

00000 00000 00000 00000  
5#12 5#12 5#12 5#12  
1 5#12 5#12 5#12 5#12  
00000 00000 00000 00000

BEAM NO 122 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN = 4200. MM FY = 414. FC = 28. MPA, SIZE = 300 X 600 MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57	5 12MM	47	3478	NO NO
2	543.	5 - 12MM	0	1144	YES NO
3	543.	5 - 12MM	288.	4200	NO YES

BEAM NO. 122 DESIGN RESULTS SHEAR

AT START SUPPORT Vu= 62.20 KNS Vc= 141.48 KNS Vs= 0.00 KNS  
Tu= 3.17 KN-MET Tc= 5.9 KN-MET Ts= 0.0 KN-MET LOAD  
NO STIRRUPS ARE REQUIRED FOR TORSION.  
REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1.  
PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272. MM C/C FOR 1563. MM

AT END SUPPORT - Vu= 58.52 KNS Vc= 141.48 KNS Vs= 0.00 KNS  
Tu= 3.17 KN-MET Tc= 5.9 KN-MET Ts= 0.0 KN-MET LOAD  
NO STIRRUPS ARE REQUIRED FOR TORSION  
REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1  
PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272. MM C/C FOR 1563. MM



STAAD SPACE

PAGE NO. 176

21J 4194X 300X 600 22J

5No12 H 543 0 TO 1144 5No12 H 543 2881 TO 4200  
 7\*12c/c272 7\*12c/c272

5No12 H 57. 547 TO 3478

00000 00000 00000 0000

5#12 5#12 5#12 5#12

5#12 5#12 5#12 5#12

00000 00000 00000 00000

# BEAM NO. 123 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200 MM FY - 414 FC 28 MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57.	5 12MM	547.	3478.	NO NO
2	543.	5 12MM	0.	1144	YES NO
3	543	5 12MM	2881.	4200	NO YES

# BEAM NO. 123 DESIGN RESULTS - SHEAR

AT START SUPPORT  $V_u = 60.12$  KNS  $V_c = 141.94$  KNS  $V_s = 0.00$  KNS  
 $T_u = 2.32$  KN-MET  $T_c = 5.9$  KN-MET  $T_s = 0.0$  KN-MET LOAD 1  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL.11.5.5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272 MM C/C FOR 1563 MM

AT END SUPPORT  $V_u = 60.60$  KNS  $V_c = 141.94$  KNS  $V_s = 0.00$  KNS  
 $T_u = 2.32$  KN-MET  $T_c = 5.9$  KN-MET  $T_s = 0.0$  KN-MET LOAD 1  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL.11.5.5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272 MM C/C FOR 1563 MM

STAAD SPACE

PAGE NO. 107

220 4199X 400X 600 230

5No.12 H 543. 0.TO 1144 5No12 H 543 2881.TC 4200  
 7\*12c/c272 7\*12c/c272

5No12 H 57 547.TO 3478

00000	00000	00000	00000
5#12	5#12	5#12	5#12
5#12	5#12	5#12	5#12
00000	00000	00000	00000

# BEAM NO. 124 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN 4200 MM FY = 414 FC = 28 MPA, SIZE = 300 X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	57.	5 - 12MM	547	3478	NO	NO
2	543	5 - 12MM	0.	1144.	YES	NO
3	543.	5 - 12MM	2881	4200	NO	YES

# BEAM NO. 124 DESIGN RESULTS - SHEAR

AT START SUPPORT Vu= 63.16 KNS Vc= 141.92 KNS Vs= 0.00 KNS  
 Tu= 0.07 KN-MET Tc= 5.9 KN-MET Ts= 0.0 KN-MET LOAD 1  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272 MM C/C FOR 1564 MM

AT END SUPPORT Vu= 57.55 KNS Vc= 141.92 KNS Vs= 0.00 KNS  
 Tu= 0.07 KN-MET Tc= 5.9 KN-MET Ts= 0.0 KN-MET LOAD 1  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272 MM C/C FOR 1564. MM

STAAD SPACE

- PAGE NO 108

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24J _____ 4200X 300X 600 _____ 441
=====
5No12 H 543 0.TO 1144 5No12 H 543 2881 TO 4200
7*12c/c272 7*12c/c272
5No12 H 57. 547.TO 3478
=====

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00.00	00000	1	00000	00000	00000
5#12	5#12		5#12	5#12	5#12
	5#12	5#12	5#12	5#12	
	00000	00000	00000	00000	

# BEAM NO. 125 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200. MM FY - 414 FC - 28 MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57.	5 - 12MM	547	3478.	NO NO
2	543.	5 - 12MM	0.	1144.	YES NO
3	543.	5 - 12MM	2531	4200	NO YES

# BEAM NO 125 DESIGN RESULTS - SHEAR

AT START SUPPORT Vu= 58.90 KNS Vc 141.80 KNS Vs 0.00 KNS  
 Tu= 2.66 KN-MET Tc= 5.9 KN MET Ts= 0.0 KN-MET LOAD 1  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL.11 5.5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272 MM C/C FOR 1564. MM

AT END SUPPORT Vu= 64.93 KNS Vc 141.80 KNS Vs 0.00 KNS  
 Tu= 2.66 KN-MET Tc= 5.9 KN MET Ts= 0.0 KN-MET LOAD 1  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT FOR SHEAR IS PER CL.11 5.5.1.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272 MM C/C FOR 1564 MM

STAAD SPACE

-- PAGE NO 109

20J 4200X 300X 600 21J

5No12 H 543. 0 TO 1144

5No12 H 543 2881 TO 4200

1\*12c/c 72

1\*12c/c 272

5No12 H 57 547 TO 3478

00000

00000

00000

00000

5#12

5#12

5#12

5#12

5#12

5#12

5#12

5#12

00000

00000

00000

00000

## BEAM NO. 126 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200. MM FY - 414 FC 28. MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	57.	5 12MM	547	3478	NO	NO
2	543	5 - 12MM	0	1144.	YES	NO
3	543	5 12MM	2881.	4200.	NC	YES

## BEAM NO. 126 DESIGN RESULTS - SHEAR

AT START SUPPORT -  $V_u = 6.96$  KNS  $V_c = 140.48$  KNS  $V_s = 0.00$  KNS $T_u = 6.98$  KN-MET  $T_c = 5.8$  KN-MET  $T_s = 9.3$  KN-MET LOAD 2

STIRRUPS ARE REQUIRED FOR TORSION.

REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1

PROVIDE 12 MM 2-LEGGED STIRRUPS AT 181. MM C/C FOR 1563. MM

ADDITIONAL LONGITUDINAL STEEL REQD FOR TORSIONAL RESISTANCE 1.77 SQ CM

AT END SUPPORT  $V_u = 66.64$  KNS  $V_c = 140.48$  KNS  $V_s = 0.00$  KNS $T_u = 6.98$  KN-MET  $T_c = 5.8$  KN-MET  $T_s = 9.3$  KN-MET LOAD 2

STIRRUPS ARE REQUIRED FOR TORSION

REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1.

PROVIDE 12 MM 2 LEGGED STIRRUPS AT 181. MM C/C FOR 1563 MM

ADDITIONAL LONGITUDINAL STEEL REQD. FOR TORSIONAL RESISTANCE 1.77 SQ.CM.

STAAD SPACE

PAGE NO. 110

337 4199A 300X 600 347

5No12 H 543, 0 TO 1144

5No12 H 543, 2881 TO 4200

10\*12c/-181

10\*12c/-181

5No12 H 57 547 TO 3478

000000	000000		000000	000000
5#12	5#12		5#12	5#12
	5#12	5#12	5#12	5#12
000000	000000	000000	000000	000000

## BEAM NO. 127 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200. MM FY - 414 FC 28. MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57.	5 12MM	547	3478.	NO NO
2	543.	5 12MM	0	1144.	YES NO
3	543.	5 12MM	2881.	4200	NO YES

## BEAM NO. 127 DESIGN RESULTS - SHEAR

AT START SUPPORT - Vu= 67.85 KNS Vc 140.63 KNS Vs 0.00 KNS  
 T1= 4.23 KN-MET Tc= 5.8 KN-MET Ts= 0.0 KN-MET LOAD 2  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL.11.5.5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272. MM C/C FOR 1563. MM

AT END SUPPORT Vu= 65.86 KNS Vc 140.63 KNS Vs= 0.00 KNS  
 T1= 4.23 KN-MET Tc= 5.8 KN-MET Ts= 0.0 KN-MET LOAD 2  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT FOR SHEAR IS PER CL.11.5.5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 272. MM C/C FOR 1563. MM

STAAD SPACE

PAGE NO. 111

32J 4.99X 10JX 600 34I

5No12 H 543 0 TO 1144 5No12 H 543 2881 TO 4200  
 7\*12C/C272 7\*12C/C272  
 5No12 H 57. 547 TO 3478

00000 1 00000 00000 00000  
 5#12 1 5#12 5#12 5#12  
 5#12 5#12 5#12 5#12  
 00000 00000 00000 00000

BEAM NO. 128 DESIGN RESULTS FLEXURE PER CODE ACI 318-05					
LEN - 4200. MM	FY - 414	FC - 28	MPA, SIZE	300. X 600. MMS	
LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57	5 12MM	547.	3478.	NO NO
2	543	5 - 12MM	0	1144	YES NO
3	543.	5 12MM	2881.	4200	NO YES

## BEAM NO. 128 DESIGN RESULTS - SHEAR

AT START SUPPORT  $V_u = 69.10$  KNS  $V_c = 161.39$  KNS  $V_s = 0.00$  KNS  
 $T_u = 1.30$  KN-MET  $T_c = 6.3$  KN MET  $T_s = 0.0$  KN MET LOAD 2  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL 11.5.1.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 22. MM C/C FOR 1563 MM

AT END SUPPORT -  $V_u = 43.03$  KNS  $V_c = 255.68$  KNS  $V_s = 0.00$  KNS  
 $T_u = 0.93$  KN-MET  $T_c = 6.2$  KN MET  $T_s = 0.0$  KN MET LOAD 1  
 STIRRUPS ARE NOT REQUIRED.

STAAD SPACE

-- PAGE NO. 112

40J 4199X 300X 600 39J

5No12 H 543. 0 TO 1144

5No12 H 543 2881 TO 4200

\*12c/c272

5No12 H 57. 547 TO 3478

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5#12

5#12

5#12

5#12

5#12

5#12

5#12

5#12

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## BEAM NO. 129 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200 MM FY - 414. FC - 28 MPA, SIZE - 300 X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	57.	5 12MM	547	3478.	NO	NO
2	543.	5 - 12MM	0	1144	YES	NO
3	543.	5 12MM	2881	4200	NO	YES

## BEAM NO. 129 DESIGN RESULTS - SHEAR

AT START SUPPORT -  $V_u = 44.10$  KNS  $V_c = 257.91$  KNS  $V_s = 0.00$  KNS $T_u = 0.39$  KN-MET  $T_c = 6.3$  KN MET  $T_s = 0.0$  KN-MET LOAD 1

STIRRUPS ARE NOT REQUIRED

AT END SUPPORT  $V_u = 67.60$  KNS  $V_c = 170.74$  KNS  $V_s = 0.00$  KNS $T_u = 0.55$  KN-MET  $T_c = 6.5$  KN MET  $T_s = 0.0$  KN-MET LOAD 2

NO STIRRUPS ARE REQUIRED FOR TORSION

REINFORCEMENT FOR SHEAR IS PER CL 11.7.5.1

PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272 MM C C FOR 1.63 MM

STAAD SPACE

PAGE NO 113

38J 4199X 300X 600 4CJ

5N12 H 543. C TO 1144 5N12 H 543 2881 TO 4200 ,

5N12 H 57 547 TO 3478

00000	00000			00000	00000
#12	#12			#12	#12
	5#12	5#12	5#12	5#12	
	00000	00000	00000	00000	

# BEAM NO. 130 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200. MM FY - 414. FC - 28. MPA, SIZE - 300. X 600 MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	5	5 - 12MM	547	3478.	NO	NO
2	543.	5 - 12MM	0.	1.44	YES	NO
3	543.	5 - 12MM	2881	4200.	NO	YES

# BEAM NO 130 DESIGN RESULTS - SHEAR

AT START SUPPORT -  $V_u = 67.21$  KNS  $V_c = 140.58$  KNS  $V_s = 0.00$  KNS  
 $T_u = 7.94$  KN-MET  $T_c = 5.8$  KN-MET  $T_s = 10.6$  KN-MET LOAD 2  
 STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT FOR SHEAR IS PER CI 11.5.5.1.  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 181. MM C/C FOR 1563 MM  
 ADDITIONAL LONGITUDINAL STEEL REQD. FOR TORSIONAL RESISTANCE = 2.01 SQ.CM.

AT END SUPPORT -  $V_u = 66.49$  KNS  $V_c = 140.58$  KNS  $V_s = 0.00$  KNS  
 $T_u = 7.94$  KN-MET  $T_c = 5.8$  KN-MET  $T_s = 10.6$  KN-MET LOAD 2  
 STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CI 11.5.5.1  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 181 MM C/C FOR 1563 MM  
 ADDITIONAL LONGITUDINAL STEEL REQD. FOR TORSIONAL RESISTANCE = 2.01 SQ.CM.



STAAD SPACE

-- PAGE NO. 114

6J \_\_\_\_\_ 4199X 300X 600 \_\_\_\_\_ 7J \_\_\_\_\_

5No12 H 543.1 C.TO 1144

5No 2 H 543.2881 TO 4200

10\*12c/c181

10\*12c/c181

5No12 H 57. 547 TO 3478

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00000

00000

5#12

5#12

5#12

5#12

5#12

5#12

5#12

5#12

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## BEAM NO. 131 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 4200. MM FY - 414 FC - 28. MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR	
					STA	END
1	57	5 12MM	547.	3478	NO	NO
2	543	5 12MM	0.	1144	YES	NO
3	543	5 - 12MM	2881	4200	NO	YES

## BEAM NO. 131 DESIGN RESULTS - SHEAR

AT START SUPPORT -  $V_u = 68.03$  KNS  $V_c = 140.44$  KNS  $V_s = 0.00$  KNS $T_u = 2.35$  KN-MET  $T_c = 5.8$  KN-MET  $T_s = 0.0$  KN-MET LOAD 2

NO STIRRUPS ARE REQUIRED FOR TORSION.

REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1.

PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272. MM C/C FOR 1564. MM

AT END SUPPORT  $V_u = 61.67$  KNS  $V_c = 140.44$  KNS  $V_s = 0.00$  KNS $T_u = 2.35$  KN-MET  $T_c = 5.8$  KN-MET  $T_s = 0.0$  KN-MET LOAD 2

NO STIRRUPS ARE REQUIRED FOR TORSION

REINFORCEMENT FOR SHEAR IS PER CL 11.5.5.1.

PROVIDE 12 MM 2-LEGGED STIRRUPS AT 272 MM C/C FOR 1,64 MM

STAAD SPACE

-- PAGE NO. 115

5J 4200X 400X 600 6J

5No12 H 543. 0 TO 1144 5No12 H 543.2881 TO 4200  
 7\*12c c272 7\*12c c272  
 5No12 H 57 547. TO 3478

00000 00000 00000 00000  
 5#12 5#12 5#12 5#12  
 5#12 5#12 5#12 5#12  
 00000 00000 00000 00000

# BEAM NO. 132 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 8000. MM FY - 414. FC 28. MPA, SIZE 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	63.	3 25MM	731	6936	NO NO
2	533	3 42MM	7	4458.	YES NO
3	537.	4 25MM	4427	8000	NO YES

# BEAM NO 132 DESIGN RESULTS - SHEAR

AT START SUPPORT Vu= 342.51 KNS Vc= 129.67 KNS Vs 194.68 KNS  
 Tu= 0.02 KN-MET Tc= 5.4 KN-MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR.  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 260 MM C/C FOR 3464 MM

AT END SUPPORT Vu= 230.94 KNS Vc= 129.67 KNS Vs 178.25 KNS  
 Tu= 0.02 KN-MET Tc= 5.4 KN-MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 260 MM C/C FOR 3464 MM

STAAD SPACE

PAGE NO 116

225 8000x 300x 600 341

3No32 H 533. 0 TO 4458 4No25 H 517.442 TO 8000  
 15\*12c/c260 14\*12c/c269  
 3No25 H 63. 731 TO 6916

000	000	000	0000	0000	0000
3#32	3#32	3#32	4#25	4#25	4#25
	3#25	3#25	4#25	3#25	
	000	000	000	000	

# BEAM NO. 133 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 8000. MM FY - 414. FC 28. MPA, SIZE - 300 X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	61.	3 - 20MM	1128	6519.	NO	NO
2	513	2 - 32MM	0	2896	YES	NO
3	539	4 - 20MM	513	8000	NO	YES

# BEAM NO 133 DESIGN RESULTS - SHEAR

AT START SUPPORT Vu= 173.19 KNS Vc= 134.83 KNS Vs 96.08 KNS  
 Tu= 0.32 KN-MET Tc= 5.6 KN-MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 270 MM C C FOR 3464. MM

AT END SUPPORT Vu= 156.96 KNS Vc= 134.8 KNS Vs 74.45 KNS  
 Tu= 0.32 KN-MET Tc= 5.6 KN-MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 270. MM C C FOR 3464. MM

STANDARD SPACE

-- PAGE NO. 117

20J 800CX 300X 600 35J

2No12 H 533 0. TO 2896 4No20 H 539 5113 TO 8000  
 4\*12c/c270 14\*12c/c270  
 3No20 H 61 1128 TO 6539

CO	OO			OOOO	OOOO
2#12	2#12			4#20	4#20
	3#20	3#20	3#20	3#20	
	OOO	OOO	OOO	OOO	

## BEAM NO. 134 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 8000. MM FY - 414. FC - 28. MPA, SIZE - 300 X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	61.	3 20MM	1155.	6511.	NO NO
2	539.	4 20MM	0	2554.	YES NO
3	537.	3 25MM	4599	8000	NO YES

## BEAM NO. 134 DESIGN RESULTS - SHEAR

AT START SUPPORT -  $V_d = 157.32$  KNS  $V_c = 134.57$  KNS  $V_s = 76.20$  KNS  
 $T_d = 0.58$  KN MET  $T_c = 5.6$  KN MET  $T_s = 0.0$  KN MET LOAD  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT IS REQUIRED FOR SHEAR.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 270. MM C/C FOR 3464 MM

AT END SUPPORT  $V_d = 168.69$  KNS  $V_c = 133.55$  KNS  $V_s = 91.37$  KNS  
 $T_d = 0.58$  KN MET  $T_c = 5.6$  KN-MET  $T_s = 0.0$  KN-MET LOAD  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT IS REQUIRED FOR SHEAR.  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 270 MM C C FOR 3464. MM

STAAD SPACE

-- PAGE NO. 118

36J 8000X 300X 600 19J

4No20 H 539.1 C.T.O 2554  
14\*12c/c2703No25 H 537.4999 TO 80^C  
1 1 14\*12c/c270

3No20 H 61.1155.TC 6511

0000 4#20	0000 4#20			000 3#25	000 3#25
	3#20 000	3#20 000	3#20 000	3#20 000	

## BEAM NO. 135 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN - 8000. MM FY - 414. FC - 28. MPA, SIZE - 300 X 600 MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	63	2 - 25MM	954.	6713	NO NO
2	539	4 - 20MM	C.	2554	YES NO
3	537	3 - 25MM	1999	8000.	NO YES

## BEAM NO 135 DESIGN RESULTS - SHEAR

AT START SUPPORT - Vu= 163.44 KNS Vc= 129.46 KNS Vs= 88.47 KNS  
 Td= 0.94 KN-MET Tc= 5.4 KN MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION.  
 REINFORCEMENT IS REQUIRED FOR SHEAR  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 269 MM C/C FOR 3464. MM

AT END SUPPORT Vu= 166.71 KNS Vc= 129.46 KNS Vs= 92.82 KNS  
 Td= 0.94 KN-MET Tc= 5.4 KN MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 269 MM C/C FOR 3464 MM

STAAD SPACE

PAGE NO 119

8J 9000X 100X 600 11

4No20 H 539.1 0.TO 2554 3No25 H 537 4999.TO 8000  
 14\*12c/c269 14\*12c c269  
 2No25 H 63. 954.TO 6713

0300	0000	000	000
4#20	4#20	3#25	1#25
	2#25	2#25	2#25
	00	00	00

## BEAM NO. 136 DESIGN RESULTS - FLEXURE PER CODE ACI 318-05

LEN 8000. MM FY - 414 FC - 28. MPA, SIZE - 500. X 800. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END
1	57.	11 - 12MM	667	7007	NO NO
2	743.	11 12MM	0	1111	YES NO
3	743.	11 12MM	6556.	8000	NO YES

## BEAM NO. 136 DESIGN RESULTS - SHEAR

AT START SUPPORT  $V_u = 148.01$  KNS  $V_c = 318.78$  KNS  $V_s = 0.00$  KNS  
 $T_u = 0.37$  KN-MET  $T_c = 19.8$  KN-MET  $T_s = 0.0$  KN-MET LOAD 2  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL.11.5.5.1  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 372 MM C/C FOR 3264. MM

AT END SUPPORT  $V_u = 166.53$  KNS  $V_c = 318.78$  KNS  $V_s = 0.00$  KNS  
 $T_u = 0.37$  KN-MET  $T_c = 19.8$  KN-MET  $T_s = 0.0$  KN-MET LOAD 2  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT FOR SHEAR IS PER CL.11.5.5.1.  
 PROVIDE 12 MM 2-LEGGED STIRRUPS AT 372 MM C/C FOR 3264 MM

STAAD SPACE

-- PAGE NO 12

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      8000X 500X 800      151
=====
11No12 H 743 0.70 1111      11No12 H 743 6556 TO 8000
10*12c/c372      10*12c c372

11No12 H 57 660 TO 7007
=====
0000000000      0000000000

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0000000000 0000000000 0000000000 0000000000

BEAM NO. 137 DESIGN RESULTS FLEXURE PER CODE ACI 318-05

LEN - 8000 MM FY - 414 FC - 28 MPA, SIZE - 300. X 600. MMS

LEVEL	HEIGHT (MM)	BAR INFO	FROM (MM)	TO (MM)	ANCHOR STA END	
1	61	3 - 20MM	1.52	6515	NO	NO
2	537	3 - 20MM	0	2668.	YES	NO
3	539	4 - 20MM	115.	8000	NO	YES

BEAM NO. 137 DESIGN RESULTS - SHEAR

AT START SUPPORT Vu= 166.77 KNS Vc= 134.22 KNS Vs= 90.81 KNS  
 Tu= 0.58 KN-MET Tc= 5.6 KN-MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 200 MM C/C FOR 3464. MM

AT END SUPPORT Vu= 157.24 KNS Vc= 134.22 KNS Vs= 72.43 KNS  
 Tu= 0.58 KN-MET Tc= 5.6 KN-MET Ts= 0.0 KN-MET LOAD 5  
 NO STIRRUPS ARE REQUIRED FOR TORSION  
 REINFORCEMENT IS REQUIRED FOR SHEAR  
 PROVIDE 12 MM 2 LEGGED STIRRUPS AT 270 MM C/C FOR 3464 MM





STAAD SPACE

PAGE NO 2104

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**COLUMN NO. 682 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 AREA OF STEEL REQUIRED = 2592.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	5	STA	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE

TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 683 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2225.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE

TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 684 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE

TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 685 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 686 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 687 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

(PROVIDE EQUAL NUMBER OF BARS ON EACH FACE)  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

PAGE NO 276

COLUMN NO. 688 DESIGN PER ACI 318-05 - AXIAL + BENDING

FY 413.7 FC - 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
ONLY MINIMUM STEEL IS REQUIRED.  
AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
TIE BAR NUMBER 12 SPACING 450.00 MM

COLUMN NO. 689 DESIGN PER ACI 318-05 - AXIAL + BENDING

FY - 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
ONLY MINIMUM STEEL IS REQUIRED  
AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE,  
TIE BAR NUMBER 12 SPACING 450.00 MM

COLUMN NO. 695 DESIGN PER ACI 318-05 - AXIAL + BENDING

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
ONLY MINIMUM STEEL IS REQUIRED.  
AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 1809 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC - 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
ONLY MINIMUM STEEL IS REQUIRED.  
AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

(PROVIDE EQUAL NUMBER OF BARS ON EACH FACE)  
TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 1816 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC - 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
ONLY MINIMUM STEEL IS REQUIRED.  
AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

(PROVIDE EQUAL NUMBER OF BARS ON EACH FACE)  
TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 1823 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
ONLY MINIMUM STEEL IS REQUIRED.  
AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

(PROVIDE EQUAL NUMBER OF BARS ON EACH FACE)  
TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

PAGE NO. 2708

---

**COLUMN NO. 1830 DESIGN PER ACI 318 05 - AXIAL + BENDING**

FY - 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

---

**COLUMN NO. 1901 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY - 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1917 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, RECT SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED 8325.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
12 - 32 MM	1.159	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

PAGE NO 2708

## =====

## COLUMN NO. 1830 DESIGN PER ACI 318-05 - AXIAL + BENDING

FY 413.7 MPa, FC 27.6 MPa, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

## =====

## COLUMN NO. 1901 DESIGN PER ACI 318-05 - AXIAL + BENDING

FY 413.7 MPa, FC 27.6 MPa, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

## =====

## COLUMN NO. 1917 DESIGN PER ACI 318-05 - AXIAL + BENDING

FY 413.7 MPa, FC 27.6 MPa, RECT SIZE 450.0 X 1850.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 8325.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
12 32 MM	1.159	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 1918 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC - 27.6 MPA, RECT SIZE - 450.0 X 1850.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 8325.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
12 32 MM	1.159	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1919 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC - 27.6 MPA, RECT SIZE 450.0 X 1850.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 8325.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
12 32 MM	1.159	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO 1920 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC - 27.6 MPA, RECT SIZE 450.0 X 1850.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 8325.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
12 32 MM	1.159	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 1963 DESIGN PER ACI 318 05 - AXIAL + BENDING**

FY 413.7 MPa 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1964 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY 413.7 MPa 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1965 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 MPa 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM



STAAD SPACE

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**COLUMN NO 1966 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE,  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO 1971 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO 1972 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO 1973 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY 413.7 MPa 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1974 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 MPa 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

(PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO 1975 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 MPa 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

(PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 1976 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1981 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1982 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 1983 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 FC = 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1984 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 FC = 27.6 MPA, SQRE SIZE = 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1985 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 FC = 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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STAAD SPACE

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**COLUMN NO. 1990 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC - 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 AREA OF STEEL REQUIRED = 2166.8 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	5	STA	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1991 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 AREA OF STEEL REQUIRED = 2166.8 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	5	STA	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO 1992 DESIGN PER ACI 318.05 - AXIAL + BENDING**

FY 413.7 FC - 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 1993 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 1994 DESIGN PER ACI 318-05 AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2011 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 400 X 450 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 2012 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 MPa, FC = 27.6 MPa, SQRE SIZE = 450.0 x 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2013 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 MPa, FC = 27.6 MPa, SQRE SIZE = 450.0 x 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2014 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 MPa, FC = 27.6 MPa, SQRE SIZE = 450.0 x 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 2015 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 FC = 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2016 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 FC = 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2017 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY = 413.7 FC = 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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STAAD SPACE

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**COLUMN NO. 2018 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC - 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2019 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC - 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2020 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC - 27.6 MPA, SQRE SIZE - 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 - 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

STAAD SPACE

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**COLUMN NO. 2021 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2022 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE)  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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**COLUMN NO. 2023 DESIGN PER ACI 318-05 - AXIAL + BENDING**

FY - 413.7 FC 27.6 MPA, SQRE SIZE 450.0 X 450.0 MMS, TIED  
 ONLY MINIMUM STEEL IS REQUIRED.  
 AREA OF STEEL REQUIRED = 2025.0 SQ. MM

BAR CONFIGURATION	REINF PCT.	LOAD	LOCATION	PHI
4 32 MM	1.589	2	END	0.650

PROVIDE EQUAL NUMBER OF BARS ON EACH FACE)  
 TIE BAR NUMBER 12 SPACING 450.00 MM

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STAAD SPACE

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## ELEMENT DESIGN SUMMARY

ELEMENT	LONG. REINF (SQ MM/MM)	MOM-X /LOAD (KN-MM/MM)	TRANS REINF (SQ MM/MM)	MOM Y /LOAD (KN-MM/MM)
FY 413.682 MPA FC 27.579 MPA COVER: 19.050 MM TH 240.000 MM				
327 TOP Longitudinal direction	Only minimum steel required			
327 BOT Longitudinal direction	Only minimum steel required			
327 TOP Transverse direction	Only minimum steel required.			
327 BOT Transverse direction	Only minimum steel required.			
327 TOP	0.432	1.22 / 5	0.432	0.64 / 5
327 BOT	0.432	0.00 / 0	0.432	0.03 /
FY 413.682 MPA FC 27.579 MPA COVER: 19.050 MM TH 240.000 MM				
328 TOP Longitudinal direction	Only minimum steel required.			
328 BOT Longitudinal direction	Only minimum steel required			
328 TOP Transverse direction	Only minimum steel required			
328 BOT Transverse direction	Only minimum steel required			
328 TOP	0.432	0.20 / 6	0.432	0.43 / 6
328 BOT	0.432	0.11 / 3	0.432	0.07 / 1
FY 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH 240.000 MM				
329 TOP Longitudinal direction	Only minimum steel required.			
329 BOT Longitudinal direction	Only minimum steel required			
329 TOP Transverse direction	Only minimum steel required			
329 BOT Transverse direction	Only minimum steel required.			
329 TOP	0.432	0.72 / 5	0.432	0.76 / 5
329 BOT	0.432	0.00 / 3	0.432	0.08 /
FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH: 240.000 MM				
330 TOP Longitudinal direction	Only minimum steel required.			
330 BOT Longitudinal direction	Only minimum steel required.			
330 TOP Transverse direction	Only minimum steel required			
330 BOT Transverse direction	Only minimum steel required.			
330 TOP	0.432	0.00 / 5	0.432	0.04 / 3
330 BOT	0.432	0.11 / 5	0.432	0.44 / 6
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM				
331 TOP Longitudinal direction	Only minimum steel required			
331 BOT Longitudinal direction	Only minimum steel required.			
331 TOP Transverse direction	Only minimum steel required			
331 BOT Transverse direction	Only minimum steel required.			
331 TOP	0.432	0.33 / 6	0.432	0.81 / 6
331 BOT	0.432	0.03 /	0.432	0.07 / 6
FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 240.000 MM				
332 TOP Longitudinal direction	Only minimum steel required			
332 BOT Longitudinal direction	Only minimum steel required			
332 TOP Transverse direction	Only minimum steel required.			
332 BOT Transverse direction	Only minimum steel required			
332 TOP	0.432	0.00 / 6	0.432	0.16 / 5
332 BOT	0.432	0.41 / 6	0.432	0.05 /
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM				
333 TOP Longitudinal direction	Only minimum steel required			

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333 BOTT Longitudinal direction - Only minimum steel required  
 333 TOP Transverse direction - Only minimum steel required.  
 333 BOTT Transverse direction - Only minimum steel required  
 333 TOP 0.432 0.00 / 6 0.432 0.00 / 5  
 BOTT 0.432 0.72 / 5 0.432 3.49 6

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 240.000 MM

334 TOP Longitudinal direction - Only minimum steel required  
 334 BOTT Longitudinal direction - Only minimum steel required  
 334 TOP Transverse direction - Only minimum steel required.  
 334 BOTT Transverse direction - Only minimum steel required  
 334 TOP 0.432 0.00 / 6 0.432 0.00 / 3  
 BOTT 0.432 0.65 / 6 0.432 0.35 6

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 160.000 MM

335 TOP Longitudinal direction - Only minimum steel required  
 335 BOTT Longitudinal direction - Only minimum steel required.  
 335 TOP Transverse direction - Only minimum steel required.  
 335 BOTT Transverse direction - Only minimum steel required.  
 335 TOP 0.288 0.00 / 6 0.288 4.97 / 5  
 BOTT 0.288 5.64 / 5 0.288 0.00 / 6

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 160.000 MM

385 TOP Longitudinal direction - Only minimum steel required  
 385 BOTT Longitudinal direction - Only minimum steel required  
 385 TOP Transverse direction - Only minimum steel required  
 385 BOTT Transverse direction - Only minimum steel required  
 385 TOP 0.288 1.26 / 5 0.288 0.00 / 5  
 BOTT 0.288 0.00 / 5 0.288 4.29 / 6

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 160.000 MM

387 TOP Longitudinal direction - Only minimum steel required.  
 387 BOTT Longitudinal direction - Only minimum steel required.  
 387 TOP Transverse direction - Only minimum steel required.  
 387 BOTT Transverse direction - Only minimum steel required.  
 387 TOP 0.288 0.00 / 5 0.288 4.24 / 5  
 BOTT 0.288 6.68 / 5 0.288 0.00 / 6

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 160.000 MM

394 TOP Longitudinal direction - Only minimum steel required.  
 394 BOTT Longitudinal direction - Only minimum steel required.  
 394 TOP Transverse direction - Only minimum steel required  
 394 BOTT Transverse direction - Only minimum steel required  
 394 TOP 0.288 0.00 / 5 0.288 4.99 / 6  
 BOTT 0.288 1.5 / 5 0.288 0.00 / 6

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 160.000 MM

397 TOP Longitudinal direction - Only minimum steel required  
 397 BOTT Longitudinal direction - Only minimum steel required  
 397 TOP Transverse direction - Only minimum steel required  
 397 BOTT Transverse direction - Only minimum steel required  
 397 TOP 0.288 5.41 / 5 0.288 0.00 / 6  
 BOTT 0.288 0.00 / 5 0.288 4.75 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER 19.050 MM TH 160.000 MM

457 TOP Longitudinal direction - Only minimum steel required

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451 BOTTL Longitudinal direction Only minimum steel required.  
 451 TOP Transverse direction Only minimum steel required  
 451 BOTTL Transverse direction Only minimum steel required  
 451 TOP 0.288 4.21 / 6 0.288 0.00 6  
 BOTTL 0.288 0.00 5 0.288 1.16 / 5

FX 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 160.000 MM  
 453 TOP : Longitudinal direction Only minimum steel required  
 453 BOTTL Longitudinal direction Only minimum steel required  
 453 TOP Transverse direction - Only minimum steel required.  
 453 BOTTL Transverse direction Only minimum steel required  
 453 TOP 0.288 3.00 / 6 0.288 1.39 / 6  
 BOTTL 0.288 4.69 6 0.288 0.00 6

FY 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 160.000 MM  
 468 BOTTL Longitudinal direction Only minimum steel required  
 468 TOP : Transverse direction - Only minimum steel required  
 468 BOTTL Transverse direction Only minimum steel required  
 468 TOP 0.293 14.41 6 0.288 3.38 6  
 BOTTL 0.288 3.03 6 0.288 3.03 5

FX 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 160.000 MM  
 536 TOP : Longitudinal direction - Only minimum steel required.  
 536 BOTTL Longitudinal direction Only minimum steel required.  
 536 TOP : Transverse direction - Only minimum steel required  
 536 TOP 0.288 0.00 / 6 0.288 0.00 / 6  
 BOTTL 0.288 0.51 / 6 0.328 14.55 / 6

FY 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 160.000 MM  
 537 TOP : Longitudinal direction - Only minimum steel required  
 537 BOTTL Longitudinal direction Only minimum steel required  
 537 TOP : Transverse direction Only minimum steel required  
 537 BOTTL Transverse direction - Only minimum steel required  
 537 TOP 0.288 0.39 / 6 0.288 3.73 / 6  
 BOTTL 0.288 0.54 / 5 0.288 0.00 / 6

Y 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 160.000 MM  
 542 TOP Longitudinal direction - Only minimum steel required  
 542 BOTTL Longitudinal direction - Only minimum steel required  
 542 TOP Transverse direction Only minimum steel required  
 542 BOTTL Transverse direction - Only minimum steel required  
 542 TOP 0.288 0.00 / 1 0.288 4.10 5  
 BOTTL 0.288 6.69 5 0.288 0.00 / 6

FY 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 240.000 MM  
 707 TOP : Longitudinal direction Only minimum steel required  
 707 BOTTL Longitudinal direction Only minimum steel required  
 707 TOP Transverse direction - Only minimum steel required  
 707 BOTTL Transverse direction Only minimum steel required.  
 707 TOP 0.432 0.22 / 5 0.432 3.03 6  
 BOTTL 0.432 3.05 1 0.432 1.69 / 6

FX 413.682 MPA FC: 27 579 MPA COVER 19.050 MM TH: 240.000 MM  
 708 TOP Longitudinal direction Only minimum steel required  
 708 BOTTL Longitudinal direction Only minimum steel required  
 708 TOP : Transverse direction Only minimum steel required

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708 BOTT: Transverse direction - Only minimum steel required.

708 TOP	0.432	0.00 /	5	0.432	0.00 /	5
BOTT	0.432	1.70 /	6	0.432	0.82 /	5

FY 413.682 MPA FC 27.59 MPA COVER 19.050 MM TH 240.000 MM

709 TOP Longitudinal direction - Only minimum steel required.

709 BOTT Longitudinal direction - Only minimum steel required.

709 TOP Transverse direction - Only minimum steel required.

709 BOTT Transverse direction - Only minimum steel required.

709 TOP	0.432	0.01 /	5	0.432	0.00 /	5
BOTT	0.432	0.65 /	6	0.432	4.55 /	6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

710 TOP Longitudinal direction - Only minimum steel required.

710 BOTT Longitudinal direction - Only minimum steel required.

710 TOP Transverse direction - Only minimum steel required.

710 BOTT Transverse direction - Only minimum steel required.

710 TOP	0.432	0.00 /	5	0.432	0.00 /	5
BOTT	0.432	3.94 /	6	0.432	0.81 /	5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

711 TOP Longitudinal direction - Only minimum steel required.

711 BOTT Longitudinal direction - Only minimum steel required.

711 TOP Transverse direction - Only minimum steel required.

711 BOTT Transverse direction - Only minimum steel required.

711 TOP	0.432	0.77 /	5	0.432	2.22 /	6
BOTT	0.432	0.00 /	6	0.432	0.00 /	5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

712 TOP Longitudinal direction - Only minimum steel required.

712 BOTT Longitudinal direction - Only minimum steel required.

712 TOP Transverse direction - Only minimum steel required.

712 BOTT Transverse direction - Only minimum steel required.

712 TOP	0.432	0.08 /	5	0.432	0.01 /	5
BOTT	0.432	1.61 /	6	0.432	0.36 /	6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

713 TOP Longitudinal direction - Only minimum steel required.

713 BOTT Longitudinal direction - Only minimum steel required.

713 TOP Transverse direction - Only minimum steel required.

713 BOTT Transverse direction - Only minimum steel required.

713 TOP	0.432	0.00 /	5	0.432	0.00 /	5
BOTT	0.432	1.08 /	5	0.432	5.61 /	6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

714 TOP Longitudinal direction - Only minimum steel required.

714 BOTT Longitudinal direction - Only minimum steel required.

714 TOP Transverse direction - Only minimum steel required.

714 BOTT Transverse direction - Only minimum steel required.

714 TOP	0.432	0.01 /	3	0.432	0.00 /	3
BOTT	0.432	0.57 /	6	0.432	4.57 /	6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

715 TOP Longitudinal direction - Only minimum steel required.

715 BOTT Longitudinal direction - Only minimum steel required.

715 TOP Transverse direction - Only minimum steel required.

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715 BOTTL Transverse direction - Only minimum steel required
715 TOP : 0.432 0.14 / 5 0.432 0.08 / 3
          BOTTL 0.432 0.09 / 1 0.432 0.88 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
716 TOP Longitudinal direction - Only minimum steel required.
716 BOTTL Longitudinal direction - Only minimum steel required.
716 TOP Transverse direction - Only minimum steel required.
716 BOTTL Transverse direction - Only minimum steel required.
716 TOP 0.432 0.00 / 5 0.432 0.00 / 3
          BOTTL 0.432 2.21 / 6 0.432 0.90 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
717 TOP Longitudinal direction - Only minimum steel required.
717 BOTTL Longitudinal direction - Only minimum steel required.
717 TOP Transverse direction - Only minimum steel required.
717 BOTTL Transverse direction - Only minimum steel required.
717 TOP 0.432 0.00 / 3 0.432 0.00 / 3
          BOTTL 0.432 0.73 / 6 0.432 5.01 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
718 TOP Longitudinal direction - Only minimum steel required.
718 BOTTL Longitudinal direction - Only minimum steel required.
718 TOP Transverse direction - Only minimum steel required.
718 BOTTL Transverse direction - Only minimum steel required.
718 TOP 0.432 0.00 / 3 0.432 0.00 / 3
          BOTTL 0.432 4.96 / 6 0.432 0.88 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
719 TOP Longitudinal direction - Only minimum steel required.
719 BOTTL Longitudinal direction - Only minimum steel required.
719 TOP Transverse direction - Only minimum steel required.
719 BOTTL Transverse direction - Only minimum steel required.
719 TOP 0.432 0.73 / 5 0.432 2.41 / 6
          BOTTL 0.432 0.00 / 6 0.432 0.00 / 5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
720 TOP Longitudinal direction - Only minimum steel required.
720 BOTTL Longitudinal direction - Only minimum steel required.
720 TOP Transverse direction - Only minimum steel required.
720 BOTTL Transverse direction - Only minimum steel required.
720 TOP 0.432 0.00 / 3 0.432 0.08 / 3
          BOTTL 0.432 2.50 / 6 0.432 0.18 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
721 TOP Longitudinal direction - Only minimum steel required.
721 BOTTL Longitudinal direction - Only minimum steel required.
721 TOP Transverse direction - Only minimum steel required.
721 BOTTL Transverse direction - Only minimum steel required.
721 TOP 0.432 0.00 / 5 0.432 0.00 / 3
          BOTTL 0.432 1.11 / 5 0.432 5.96 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
722 TOP Longitudinal direction - Only minimum steel required.
722 BOTTL Longitudinal direction - Only minimum steel required.
722 TOP Transverse direction - Only minimum steel required.

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722 BOT Transverse direction Only minimum steel required
722 TOP 0.432 0.01 / 3 0.432 0.00 / 3
      BOT 0.432 0.12 / 6 0.432 5.59 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
723 TOP Longitudinal direction Only minimum steel required.
723 BOT Longitudinal direction Only minimum steel required.
723 TOP Transverse direction Only minimum steel required
723 BOT Transverse direction Only minimum steel required
723 TOP 0.432 0.03 / 2 0.432 0.16 / 3
      BOT 0.432 0.18 / 6 0.432 2.29 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
724 TOP Longitudinal direction Only minimum steel required
724 BOT Longitudinal direction Only minimum steel required.
724 TOP Transverse direction Only minimum steel required
724 BOT Transverse direction Only minimum steel required.
724 TOP 0.432 0.04 / 3 0.432 0.00 / 3
      BOT 0.432 2.16 / 6 0.432 0.86 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
725 TOP Longitudinal direction - Only minimum steel required.
725 BOT Longitudinal direction - Only minimum steel required
725 TOP Transverse direction Only minimum steel required
725 BOT Transverse direction Only minimum steel required
725 TOP 0.432 0.03 / 3 0.432 0.00 / 3
      BOT 0.432 0.11 / 6 0.432 7.09 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
726 TOP Longitudinal direction Only minimum steel required
726 BOT Longitudinal direction - Only minimum steel required
726 TOP Transverse direction Only minimum steel required
726 BOT Transverse direction Only minimum steel required
726 TOP 0.432 0.01 / 3 0.432 0.00 / 3
      BOT 0.432 5.83 / 6 0.432 1.01 / 5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
727 TOP Longitudinal direction Only minimum steel required
727 BOT Longitudinal direction Only minimum steel required
727 TOP Transverse direction Only minimum steel required
727 BOT Transverse direction Only minimum steel required
727 TOP 0.432 0.59 / 5 0.432 3.30 / 6
      BOT 0.432 7.00 / 6 0.432 7.07 / 5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
728 TOP Longitudinal direction Only minimum steel required
728 BOT Longitudinal direction - Only minimum steel required
728 TOP Transverse direction Only minimum steel required
728 BOT Transverse direction Only minimum steel required
728 TOP 0.432 0.00 / 5 0.432 0.14 / 6
      BOT 0.432 2.98 / 6 0.432 0.31 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM
729 TOP Longitudinal direction Only minimum steel required.
729 BOT Longitudinal direction Only minimum steel required
729 TOP Transverse direction Only minimum steel required

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729 BOTT Transverse direction - Only minimum steel required  
 729 TOP 0.432 0.00 / 5 0.432 0.00 / 5  
 BOTT 0.432 1.18 6 0.432 8.91 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 240.000 MM

730 TOP Longitudinal direction - Only minimum steel required  
 730 BOTT Longitudinal direction - Only minimum steel required  
 730 TOP Transverse direction - Only minimum steel required  
 730 BOTT Transverse direction - Only minimum steel required  
 730 TOP 0.432 0.00 / 5 0.432 0.00 / 5  
 BOTT 0.432 0.93 / 6 0.432 6.46 / 6

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM

731 TOP Longitudinal direction - Only minimum steel required  
 731 BOTT Longitudinal direction - Only minimum steel required  
 731 TOP Transverse direction - Only minimum steel required  
 731 TOP 0.288 0.00 / 5 0.288 0.00 / 5  
 BOTT 0.288 8.24 5 0.432 14.69 / 5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM

732 TOP Longitudinal direction - Only minimum steel required  
 732 BOTT Longitudinal direction - Only minimum steel required  
 732 TOP Transverse direction - Only minimum steel required  
 732 BOTT Transverse direction - Only minimum steel required  
 732 TOP 0.288 0.00 / 5 0.288 0.00 / 5  
 BOTT 0.288 2.32 / 5 0.288 11.05

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM

733 TOP Longitudinal direction - Only minimum steel required  
 733 BOTT Longitudinal direction - Only minimum steel required  
 733 TOP Transverse direction - Only minimum steel required  
 733 BOTT Transverse direction - Only minimum steel required  
 733 TOP 0.288 0.00 / 5 0.288 0.00 / 5  
 BOTT 0.288 1.45 / 5 0.288 9.83

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM

734 TOP Longitudinal direction - Only minimum steel required  
 734 BOTT Longitudinal direction - Only minimum steel required  
 734 TOP Transverse direction - Only minimum steel required  
 734 BOTT Transverse direction - Only minimum steel required  
 734 TOP 0.288 0.00 / 5 0.288 0.43 / 5  
 BOTT 0.288 4.19 / 5 0.288 2.30 / 5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM

735 TOP Longitudinal direction - Only minimum steel required  
 735 BOTT Longitudinal direction - Only minimum steel required  
 735 TOP Transverse direction - Only minimum steel required  
 735 BOTT Transverse direction - Only minimum steel required  
 735 TOP 0.288 1.73 6 0.288 0.64 / 5  
 BOTT 0.288 0.00 5 0.288 0.00 / 5

FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM

736 TOP Longitudinal direction - Only minimum steel required  
 736 BOTT Longitudinal direction - Only minimum steel required  
 736 TOP Transverse direction - Only minimum steel required  
 736 BOTT Transverse direction - Only minimum steel required

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736 TOP	0.288	1.64 /	5	0.288	0.83 /	
BOTT	0.288	0.00 /	5	0.288	0.00 /	
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
737 TOP	Longitudinal direction - Only minimum steel required.					
737 BOTT	Longitudinal direction - Only minimum steel required.					
737 TOP	Transverse direction - Only minimum steel required.					
737 BOTT	Transverse direction - Only minimum steel required.					
737 TOP	0.288	1.50 /	6	0.288	6.61 /	
BOTT	0.288	0.18 /	3	0.288	0.00 /	
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
738 TOP	Longitudinal direction - Only minimum steel required.					
738 BOTT	Longitudinal direction - Only minimum steel required.					
738 TOP	Transverse direction - Only minimum steel required.					
738 BOTT	Transverse direction - Only minimum steel required.					
738 TOP	0.288	3.81 /	5	0.288	6.68 /	5
BOTT	0.288	0.00 /	3	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
739 TOP	Longitudinal direction - Only minimum steel required.					
739 BOTT	Longitudinal direction - Only minimum steel required.					
739 TOP	Transverse direction - Only minimum steel required.					
739 BOTT	Transverse direction - Only minimum steel required.					
739 TOP	0.288	3.98 /	5	0.288	5.58 /	5
BOTT	0.288	0.00 /	3	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
740 TOP	Longitudinal direction - Only minimum steel required.					
740 BOTT	Longitudinal direction - Only minimum steel required.					
740 TOP	Transverse direction - Only minimum steel required.					
740 BOTT	Transverse direction - Only minimum steel required.					
740 TOP	0.288	2.68 /	6	0.288	7.93 /	5
BOTT	0.288	0.00 /	3	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
741 TOP	Longitudinal direction - Only minimum steel required.					
741 BOTT	Longitudinal direction - Only minimum steel required.					
741 TOP	Transverse direction - Only minimum steel required.					
741 BOTT	Transverse direction - Only minimum steel required.					
741 TOP	0.288	4.76 /	5	0.288	7.98 /	5
BOTT	0.288	0.00 /	3	0.288	0.00 /	
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
742 TOP	Longitudinal direction - Only minimum steel required.					
742 BOTT	Longitudinal direction - Only minimum steel required.					
742 TOP	Transverse direction - Only minimum steel required.					
742 BOTT	Transverse direction - Only minimum steel required.					
742 TOP	0.288	4.59 /	5	0.288	6.70 /	5
BOTT	0.288	0.00 /	3	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
743 TOP	Longitudinal direction - Only minimum steel required.					
743 BOTT	Longitudinal direction - Only minimum steel required.					
743 TOP	Transverse direction - Only minimum steel required.					
743 BOTT	Transverse direction - Only minimum steel required.					

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744 TOP   0.288      3.00 /   5      0.288      2.22 /   5
      BOTT   0.288      3.53 /   5      0.288      0.70 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.020 MM
744 TOP : Longitudinal direction - Only minimum steel required.
744 BOTT: Longitudinal direction - Only minimum steel required.
744 TOP : Transverse direction - Only minimum steel required.
744 BOTT: Transverse direction - Only minimum steel required.
744 TOP   0.288      1.64 /   6      0.288      1.98 /   5
      BOTT   0.288      0.70 /   5      0.288      0.00 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.000 MM
745 TOP : Longitudinal direction - Only minimum steel required.
745 BOTT: Longitudinal direction - Only minimum steel required.
745 TOP : Transverse direction - Only minimum steel required.
745 BOTT: Transverse direction - Only minimum steel required.
745 TOP   0.288      2.10 /   5      0.288      1.76 /   5
      BOTT   0.288      0.00 /   5      0.288      0.00 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.000 MM
746 TOP : Longitudinal direction - Only minimum steel required.
746 BOTT: Longitudinal direction - Only minimum steel required.
746 TOP : Transverse direction - Only minimum steel required.
746 TOP   0.288      0.00 /   5      0.288      0.00 /   5
      BOTT   0.288      8.72 /   5      0.288      15.38 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.000 MM
747 TOP : Longitudinal direction - Only minimum steel required.
747 BOTT: Longitudinal direction - Only minimum steel required.
747 TOP : Transverse direction - Only minimum steel required.
747 BOTT: Transverse direction - Only minimum steel required.
747 TOP   0.288      0.07 /   5      0.288      0.07 /   5
      BOTT   0.288      2.47 /   5      0.288      11.86 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.000 MM
748 TOP : Longitudinal direction - Only minimum steel required.
748 BOTT: Longitudinal direction - Only minimum steel required.
748 TOP : Transverse direction - Only minimum steel required.
748 BOTT: Transverse direction - Only minimum steel required.
748 TOP   0.288      0.00 /   5      0.288      0.00 /   5
      BOTT   0.288      1.27 /   5      0.288      10.50 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.000 MM
749 TOP : Longitudinal direction - Only minimum steel required.
749 BOTT: Longitudinal direction - Only minimum steel required.
749 TOP : Transverse direction - Only minimum steel required.
749 BOTT: Transverse direction - Only minimum steel required.
749 TOP   0.288      5.23 /   5      0.288      5.42 /   5
      BOTT   0.288      0.00 /   5      0.288      0.00 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      187.000 MM
750 TOP : Longitudinal direction - Only minimum steel required.
750 BOTT: Longitudinal direction - Only minimum steel required.
750 TOP : Transverse direction - Only minimum steel required.
750 BOTT: Transverse direction - Only minimum steel required.

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750 TOP	0.288	0.29	5	0.288	4.09	5
BOTT	0.288	0.00	5	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
751 TOP	Longitudinal direction - Only minimum steel required					
751 BOTT	Longitudinal direction - Only minimum steel required					
751 TOP	Transverse direction - Only minimum steel required					
751 BOTT	Transverse direction - Only minimum steel required					
751 TOP	0.288	0.00 /	5	0.288	1.00 /	6
BOTT	0.288	0.00	5	0.288	0.00	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
752 TOP	Longitudinal direction - Only minimum steel required					
752 BOTT	Longitudinal direction - Only minimum steel required					
752 TOP	Transverse direction - Only minimum steel required					
752 BOTT	Transverse direction - Only minimum steel required					
752 TOP	0.288	6.10 /	5	0.288	6.52	5
BOTT	0.288	0.00	5	0.288	0.00	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
753 TOP	Longitudinal direction - Only minimum steel required					
753 BOTT	Longitudinal direction - Only minimum steel required					
753 TOP	Transverse direction - Only minimum steel required					
753 BOTT	Transverse direction - Only minimum steel required					
753 TOP	0.288	0.40	5	0.288	5.20 /	5
BOTT	0.288	0.00	5	0.288	0.00	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
754 TOP	Longitudinal direction - Only minimum steel required					
754 BOTT	Longitudinal direction - Only minimum steel required					
754 TOP	Transverse direction - Only minimum steel required					
754 BOTT	Transverse direction - Only minimum steel required					
754 TOP	0.288	0.00 /	5	0.288	2.79	6
BOTT	0.288	0.00 /	5	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
755 TOP	Longitudinal direction - Only minimum steel required					
755 BOTT	Longitudinal direction - Only minimum steel required					
755 TOP	Transverse direction - Only minimum steel required					
755 BOTT	Transverse direction - Only minimum steel required					
755 TOP	0.288	5.66 /	5	0.288	4.12 /	6
BOTT	0.288	0.00	5	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
756 TOP	Longitudinal direction - Only minimum steel required					
756 BOTT	Longitudinal direction - Only minimum steel required					
756 TOP	Transverse direction - Only minimum steel required					
756 BOTT	Transverse direction - Only minimum steel required					
756 TOP	0.288	0.4 /	1	0.288	3.22	6
BOTT	0.288	0.16	2	0.288	0.00 /	5
FY 413.682 MPA FC, 27.579 MPA COVER 19.050 MM TH 160.000 MM						
757 TOP	Longitudinal direction - Only minimum steel required					
757 BOTT	Longitudinal direction - Only minimum steel required					
757 TOP	Transverse direction - Only minimum steel required					
757 BOTT	Transverse direction - Only minimum steel required					

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757 TOP	0.288	0 30 /	1	0.288	1.1 /	6
BOTT:	0.288	11 11 /	5	0.288	0 01 /	3

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM		
758 TOP	Longitudinal direction - Only minimum steel required.					
758 BOTT	Longitudinal direction - Only minimum steel required.					
758 TOP	Transverse direction - Only minimum steel required.					
758 BOTT	Transverse direction - Only minimum steel required.					
758 TOP	0.288	1 14 /	6	0.288	0 00 /	6
BOTT:	0.288	0 01 /	3	0.288	11 95 /	5

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM		
759 TOP	Longitudinal direction - Only minimum steel required.					
759 BOTT	Longitudinal direction - Only minimum steel required.					
759 TOP	Transverse direction - Only minimum steel required.					
759 BOTT	Transverse direction - Only minimum steel required.					
759 TOP	0.288	2 79 /	6	0.288	0.00 /	6
BOTT	0.288	0 00 /	3	0.288	11 67 /	5

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM		
760 TOP	Longitudinal direction - Only minimum steel required.					
760 BOTT	Longitudinal direction - Only minimum steel required.					
760 TOP	Transverse direction - Only minimum steel required.					
760 BOTT	Transverse direction - Only minimum steel required.					
760 TOP	0.288	1 74 /	6	0.288	0 00 /	6
BOTT:	0.288	0 00 /	3	0.288	11 00 /	5

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM		
761 TOP	Longitudinal direction - Only minimum steel required.					
761 BOTT	Longitudinal direction - Only minimum steel required.					
761 TOP	Transverse direction - Only minimum steel required.					
761 BOTT	Transverse direction - Only minimum steel required.					
761 TOP	0.288	3.43 /	6	0.288	0 02 /	5
BOTT	0.288	0 00 /	3	0.288	0 33 /	5

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM		
762 TOP	Longitudinal direction - Only minimum steel required.					
762 BOTT	Longitudinal direction - Only minimum steel required.					
762 TOP	Transverse direction - Only minimum steel required.					
762 BOTT	Transverse direction - Only minimum steel required.					
762 TOP	0.288	5 42 /	5	0.288	0 17 /	5
BOTT	0.288	0 02 /	3	0.288	0 03 /	2

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM		
763 TOP	Longitudinal direction - Only minimum steel required.					
763 BOTT	Longitudinal direction - Only minimum steel required.					
763 TOP	Transverse direction - Only minimum steel required.					
763 BOTT	Transverse direction - Only minimum steel required.					
763 TOP	0.288	4.22 /	5	0.288	0.13 /	5
BOTT	0.288	0.00 /	3	0.288	0.03 /	2

FY	413.682 MPA FC	27.579 MPA COVER	19.050 MM TH	160.000 MM
764 TOP	Longitudinal direction - Only minimum steel required.			
764 BOTT	Longitudinal direction - Only minimum steel required.			
764 TOP	Transverse direction - Only minimum steel required.			
764 BOTT	Transverse direction - Only minimum steel required.			

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64 TOP	0.288	4.71 /	6	0.288	5.94 /	5
64 BOTT	0.288	0.00 /	3	0.288	0.00 /	1
FY 413 682 MPA FC 27 579 MPA COVER 19 250 MM TH 160 000 MM						
765 TOP	Longitudinal direction		Only minimum steel required			
765 BOTT	Longitudinal direction		Only minimum steel required			
765 TOP	Transverse direction		Only minimum steel required			
765 BOTT	Transverse direction		Only minimum steel required			
765 TOP	0.288	7.02 /	5	0.288	6.14 /	5
765 BOTT	0.288	0.00 /	3	0.288	0.00 /	1
FY 413 682 MPA FC 27 579 MPA COVER 19 250 MM TH 160 000 MM						
766 TOP	Longitudinal direction		Only minimum steel required			
766 BOTT	Longitudinal direction		Only minimum steel required			
766 TOP	Transverse direction		Only minimum steel required			
766 BOTT	Transverse direction		Only minimum steel required			
766 TOP	0.288	5.74 /	5	0.288	5.48 /	5
766 BOTT	0.288	0.00 /	3	0.288	0.00 /	1
FY 413 682 MPA FC 27 579 MPA COVER 19 250 MM TH 160 000 MM						
767 TOP	Longitudinal direction		Only minimum steel required			
767 BOTT	Longitudinal direction		Only minimum steel required			
767 TOP	Transverse direction		Only minimum steel required			
767 BOTT	Transverse direction		Only minimum steel required			
767 TOP	0.288	0.00 /	5	0.288	0.00 /	5
767 BOTT	0.288	2.38 /	5	0.288	2.90 /	5
FY 413 682 MPA FC 27 579 MPA COVER 19 250 MM TH 160 000 MM						
768 TOP	Longitudinal direction		Only minimum steel required			
768 BOTT	Longitudinal direction		Only minimum steel required			
768 TOP	Transverse direction		Only minimum steel required			
768 BOTT	Transverse direction		Only minimum steel required			
768 TOP	0.288	0.00 /	5	0.288	0.00 /	5
768 BOTT	0.288	2.63 /	5	0.288	3.78 /	5
FY 413 682 MPA FC 27.5 579 MPA COVER 19 250 MM TH 160 000 MM						
769 TOP	Longitudinal direction		Only minimum steel required			
769 BOTT	Longitudinal direction		Only minimum steel required			
769 TOP	Transverse direction		Only minimum steel required			
769 BOTT	Transverse direction		Only minimum steel required			
769 TOP	0.288	0.00 /	5	0.288	0.00 /	5
769 BOTT	0.288	7.56 /	5	0.288	4.65 /	5
FY 413 682 MPA FC 27 579 MPA COVER 19 250 MM TH 160 000 MM						
770 TOP	Longitudinal direction		Only minimum steel required			
770 BOTT	Longitudinal direction		Only minimum steel required			
770 TOP	Transverse direction		Only minimum steel required			
770 BOTT	Transverse direction		Only minimum steel required			
770 TOP	0.288	0.00 /	5	0.288	0.00 /	5
770 BOTT	0.288	2.70 /	5	0.288	0.45 /	5
FY 413 682 MPA FC 27 579 MPA COVER 19 250 MM TH 160 000 MM						
771 TOP	Longitudinal direction		Only minimum steel required			
771 BOTT	Longitudinal direction		Only minimum steel required			
771 TOP	Transverse direction		Only minimum steel required			
771 BOTT	Transverse direction		Only minimum steel required			

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771 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      1.63 /   5      0.288      0.51 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
772 TOP      Longitudinal direction - Only minimum steel required
772 BOTT      Longitudinal direction - Only minimum steel required
772 TOP      Transverse direction - Only minimum steel required
772 BOTT      Transverse direction - Only minimum steel required.
772 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      1.24 /   5      0.288      1.17 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
773 TOP      Longitudinal direction - Only minimum steel required
773 BOTT      Longitudinal direction - Only minimum steel required.
773 TOP      Transverse direction - Only minimum steel required.
773 BOTT      Transverse direction - Only minimum steel required
773 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      5.02 /   5      0.288      4.82 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
774 TOP      Longitudinal direction - Only minimum steel required
774 BOTT      Longitudinal direction - Only minimum steel required
774 TOP      Transverse direction - Only minimum steel required
774 BOTT      Transverse direction - Only minimum steel required
774 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      1.33 /   6      0.288      0.30 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
775 TOP      Longitudinal direction - Only minimum steel required
775 BOTT      Longitudinal direction - Only minimum steel required
775 TOP      Transverse direction - Only minimum steel required.
775 BOTT      Transverse direction - Only minimum steel required
775 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      6.22 /   5      0.288      0.06 /   3

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
776 TOP      Longitudinal direction - Only minimum steel required
776 BOTT      Longitudinal direction - Only minimum steel required
776 TOP      Transverse direction - Only minimum steel required
776 BOTT      Transverse direction - Only minimum steel required
776 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      1.42 /   5      0.288      4.55 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
777 TOP      Longitudinal direction - Only minimum steel required.
777 BOTT      Longitudinal direction - Only minimum steel required
777 TOP      Transverse direction - Only minimum steel required
777 BOTT      Transverse direction - Only minimum steel required
777 TOP      0.288      0.00 /   5      0.288      0.00 /   6
      BOTT      0.288      2.62 /   5      0.288      3.58 /   5

      FY      413.682 MPA FC      27.579 MPA COVER      19.050 MM TH      160.000 MM
778 TOP      Longitudinal direction - Only minimum steel required
778 BOTT      Longitudinal direction - Only minimum steel required
778 TOP      Transverse direction - Only minimum steel required.
778 BOTT      Transverse direction - Only minimum steel required

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778 TOP	0.288	0.00 /	5	0.288	0.00 /	6
BOTT	0.288	1.49 /	5	0.288	2.12 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
779 TOP	Longitudinal direction Only minimum steel required					
779 BOTT	Longitudinal direction - Only minimum steel required					
779 TOP	Transverse direction Only minimum steel required					
779 BOTT	Transverse direction - Only minimum steel required					
779 TOP :	0.288	0.00 /	5	0.288	0.00 /	6
BOTT	0.288	1.49 /	5	0.288	2.12 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
780 TOP	Longitudinal direction Only minimum steel required					
780 BOTT	Longitudinal direction - Only minimum steel required					
780 TOP	Transverse direction Only minimum steel required					
780 BOTT	Transverse direction - Only minimum steel required					
780 TOP :	0.288	0.00 /	5	0.288	0.00 /	6
BOTT	0.288	1.70 /	5	0.288	0.47 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
781 TOP	Longitudinal direction Only minimum steel required					
781 BOTT	Longitudinal direction - Only minimum steel required					
781 TOP	Transverse direction Only minimum steel required					
781 BOTT	Transverse direction - Only minimum steel required					
781 TOP :	0.288	0.00 /	5	0.288	0.15 /	6
BOTT	0.288	2.48 /	5	0.288	0.37 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
782 TOP	Longitudinal direction Only minimum steel required					
782 BOTT	Longitudinal direction - Only minimum steel required					
782 TOP	Transverse direction - Only minimum steel required					
782 BOTT	Transverse direction - Only minimum steel required					
782 TOP :	0.288	0.00 /	5	0.288	0.69 /	6
BOTT	0.288	6.14 /	5	0.288	0.06 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
783 TOP	Longitudinal direction Only minimum steel required					
783 BOTT	Longitudinal direction - Only minimum steel required					
783 TOP	Transverse direction - Only minimum steel required					
783 BOTT	Transverse direction - Only minimum steel required					
783 TOP :	0.288	0.00 /	5	0.288	0.00 /	6
BOTT	0.288	1.47 /	5	0.288	0.37 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
784 TOP	Longitudinal direction Only minimum steel required					
784 BOTT	Longitudinal direction - Only minimum steel required					
784 TOP	Transverse direction - Only minimum steel required					
784 BOTT	Transverse direction - Only minimum steel required					
784 TOP :	0.288	0.00 /	5	0.288	0.00 /	6
BOTT	0.288	5.61 /	5	0.288	3.91 /	5
FY 413.682 MPA FC 27.579 MPA COVER 19.050 MM TH 160.000 MM						
785 TOP	Longitudinal direction Only minimum steel required					
785 BOTT	Longitudinal direction - Only minimum steel required					
785 TOP	Transverse direction Only minimum steel required					
785 BOTT	Transverse direction - Only minimum steel required					

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785 TOP : 0.288 0.00 / 5 0.288 0.00 / 6  
 BOTT: 0.288 2.46 / 5 0.288 3.94 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 786 TOP : Longitudinal direction - Only minimum steel required.  
 786 BOTT: Longitudinal direction - Only minimum steel required.  
 786 TOP : Transverse direction - Only minimum steel required.  
 786 BOTT: Transverse direction - Only minimum steel required.  
 786 TOP : 0.288 0.00 / 5 0.288 0.00 / 6  
 BOTT: 0.288 0.39 / 5 0.288 4.92 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 787 TOP : Longitudinal direction - Only minimum steel required.  
 787 BOTT: Longitudinal direction - Only minimum steel required.  
 787 TOP : Transverse direction - Only minimum steel required.  
 787 BOTT: Transverse direction - Only minimum steel required.  
 787 TOP : 0.288 0.80 / 6 0.288 0.00 / 6  
 BOTT: 0.288 0.02 / 3 0.288 5.41 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 788 TOP : Longitudinal direction - Only minimum steel required.  
 788 BOTT: Longitudinal direction - Only minimum steel required.  
 788 TOP : Transverse direction - Only minimum steel required.  
 788 BOTT: Transverse direction - Only minimum steel required.  
 788 TOP : 0.288 0.00 / 6 0.288 0.00 / 6  
 BOTT: 0.288 1.93 / 5 0.288 1.93 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 789 TOP : Longitudinal direction - Only minimum steel required.  
 789 BOTT: Longitudinal direction - Only minimum steel required.  
 789 TOP : Transverse direction - Only minimum steel required.  
 789 BOTT: Transverse direction - Only minimum steel required.  
 789 TOP : 0.288 0.00 / 6 0.288 0.00 / 6  
 BOTT: 0.288 0.60 / 6 0.288 1.49 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 790 TOP : Longitudinal direction - Only minimum steel required.  
 790 BOTT: Longitudinal direction - Only minimum steel required.  
 790 TOP : Transverse direction - Only minimum steel required.  
 790 BOTT: Transverse direction - Only minimum steel required.  
 790 TOP : 0.288 0.00 / 6 0.288 0.00 / 6  
 BOTT: 0.288 0.71 / 6 0.288 1.53 / 6

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 791 TOP : Longitudinal direction - Only minimum steel required.  
 791 BOTT: Longitudinal direction - Only minimum steel required.  
 791 TOP : Transverse direction - Only minimum steel required.  
 791 BOTT: Transverse direction - Only minimum steel required.  
 791 TOP : 0.288 0.00 / 6 0.288 0.00 / 6  
 BOTT: 0.288 2.07 / 5 0.288 4.49 / 5

FY: 413.682 MPA FC: 27.579 MPA COVER: 19.050 MM TH: 160.000 MM  
 792 TOP : Longitudinal direction - Only minimum steel required.  
 792 BOTT: Longitudinal direction - Only minimum steel required.  
 792 TOP : Transverse direction - Only minimum steel required.  
 792 BOTT: Transverse direction - Only minimum steel required.

# الفصل الخامس

## الخلاصة :-

ان التصميم الانشائي للمباني هو من صميم عمل المهندس المدني والذي يعكس فيه كل امكانياته وخبراته في التصميم الانشائي للوصول الى الشكل الامثل من خلال استخدام المواد مع توفير الدقة والجمالية بموجب المواصفات المطلوبة مع التوازن الامثل بين الوقت والكلفة والامان .

تم اعتماد برنامج STAAD pro.v8i في تنفيذ المشروع لانشاء بناية ٤ طوابق لقسم دراسي لاحد الجامعات وكانت النتائج جيدة ومطابقة للمواصفات القياسية مما يدل على دقة البرامج واهميتها في مجال الهندسة المدنية.

ان الاعتماد فقط على البرامج الجاهزة في التصميم الانشائي بالرغم من الدقة والسرعة العاليتين في التنفيذ التي تمتلكها تلك البرامج تكون غير كافية وجازمة من دون ان يكون لدى المهندس الخبرة الكافية و الحس الهندسي اللازم للتأكد من صحة تلك النتائج وملائمتها للواقع لان التحليل والتصميم باستخدام البرامج قد يصاحبه بعض الاخطاء نيجة لسهو في الادخال او سوء تقدير للنتائج وقد صادفتني مثل تلك المشكلة اثناء ادخال الاحمال حيث قمت بادخال الحمل مرتين لاحد الطوابق سهوا ونتيجة لذلك كانت كمية حديد التسليح كبيرة ولولا نصيحة الدكتور المشرف لما استطعت معرفة الخطا الحاصل في التصميم وهذا يدل على ان من اهم عناصر التصميم السريع والدقيق هما الخبرة العملية والدقة في استخدام البرامج اي ان احدهما يكمل الاخر ، نحن في هذه المرحلة اخذنا فكرة عن استخدام البرامج في التحليل و التصميم و لكن الخبرة لايمكن اكتسابها الا بالعمل الميداني ومواكبة التطور العلمي في هذا المجال .

